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THESIS

A CIRCUIT MODEL FOR TWO-PATH
CUTOFF WAVEGUIDE
DIELECTRIC RESONATOR FILTERS

by

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March 1992

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This thesis describes the development of a CAD circuit model for two-path cutoff waveguide dielectric resonator filters. The model was verified using published data of known designs in X-band waveguide. Results from the model agree very well with experimental data.

Also, a method for designing this type of filter is proposed. It makes use of commercially available CAD software. An example of the design process is given, along with experimental data obtained from a filter manufactured according to the design.

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A Circuit Model for Two-Path
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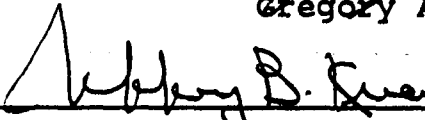
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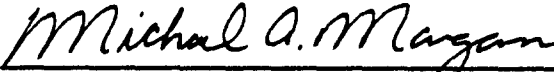from the

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ABSTRACT

This thesis describes the development of a CAD circuit model for two-path cutoff waveguide dielectric resonator filters. The model was verified using published data of known designs in X-band waveguide. Results from the model agree very well with experimental data.

Also, a method for designing this type of filter is proposed. It makes use of commercially available CAD software. An example of the design procedure is given, along with experimental data obtained from a filter manufactured according to the design.

TABLE OF CONTENTS

LIST OF TABLES

LIST OF FIGURES

ACKNOWLEDGEMENTS

I. INTRODUCTION

A. BACKGROUND

A two-path cutoff waveguide dielectric resonator filter is a new type of evanescent-mode waveguide bandpass filter consisting of dielectric resonators incorporated in two parallel cutoff waveguide paths. The two paths are realized by a complete *E*-plane bifurcation of a standard size rectangular waveguide. The resonators are realized using dielectric blocks of low permittivity within the cutoff sections. This type of filter was first proposed by Shigesawa, *et al.*, in 1986 [Ref. 1] and modified by the same authors in 1989 [Ref. 2]. However, evanescent-mode waveguide dielectric resonator filters using low permittivity dielectric material were first proposed much earlier.

The basic idea behind these structures is that a bandpass filter can be constructed from a series of resonators. Each resonator can be pictured as a short section of transmission line terminated at both ends with a large discontinuity. The frequency of resonance depends on the length of the transmission line and the discontinuity elements. The resonators in the subject filters are the dielectric blocks in the below cutoff sections. The

1

dielectric drops the cutoff frequency to well below the desired passband frequencies, hence making a short propagating section. The discontinuities are the below cutoff air-filled sections which behave like large inductive susceptances.

B. OBJECTIVES

The objective of this thesis is to describe a CAD compatible equivalent circuit model for two-path cutoff waveguide dielectric resonator filters. The model is verified by comparing its frequency response to published experimental data obtained from proven designs.

The secondary objective is to describe a design method using the model and the resident optimizers available in the microwave circuit CAD software package *Touchstone* available from *EEsof*. Design by optimizers is faster and more reliable than the design methods described in previous work.

II. PREVIOUS DESIGNS

A. ONE-PATH FILTERS

A typical early design of evanescent-mode waveguide
dielectric resonator filters using dielectrics with low
relative permittivity is given by Shih and Gray [Ref. 3].
The proposed structure was then a section of below cutoff
rectangular waveguide loaded with dielectric resonators such
that short blocks of dielectric material completely filled
the cross section of the waveguide. This was coupled to the
external circuit (a larger rectangular waveguide) via a
double-step waveguide junction. The devices that were built
used WR-42 as the larger waveguide and WR-22 as the smaller
guide. A typical configuration is shown in Fig. 1.

This design has several drawbacks. The fist being the
double step junction between different sizes of waveguide.
A junction like this is not easy to manufacture, susceptible
to stress failure, and is difficult to reproduce with
reasonable tolerances. Also, positioning the dielectric
blocks within the smaller section accurately is almost
impossible. Not all the drawbacks are mechanical in nature,
however. The cutoff characteristics of the device allow
higher frequencies to couple into the structure just
slightly more efficiently than the lower frequencies. This

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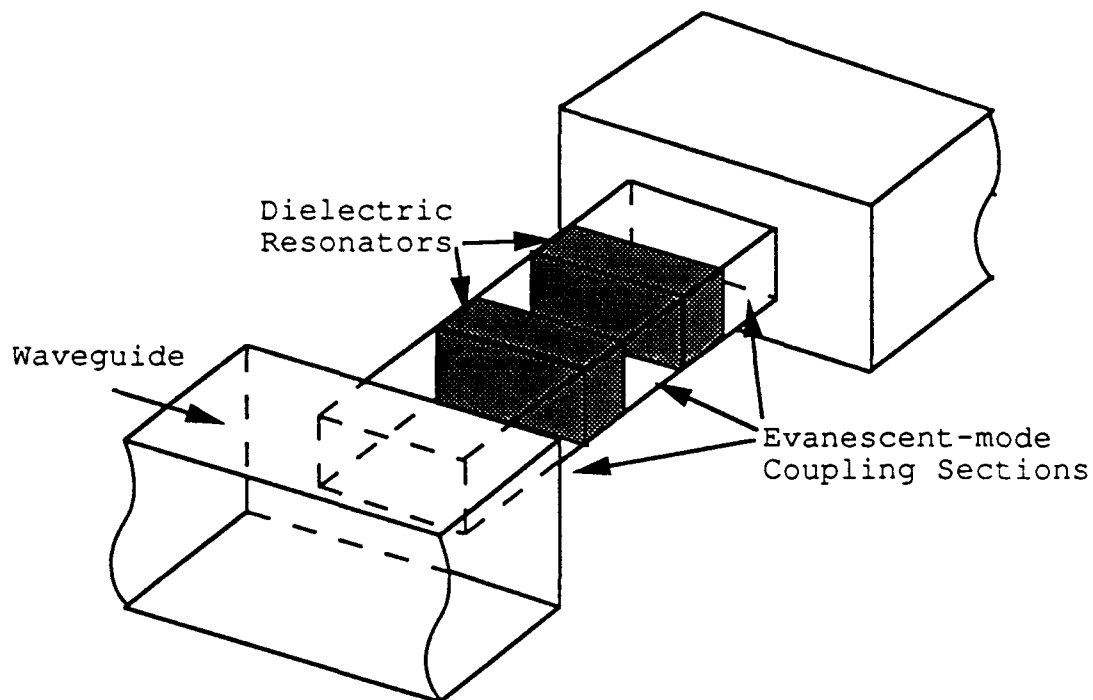
Figure 1. **Evanescent-mode waveguide dielectric resonator filter**

leads to asymmetric stopband characteristics. That is, the upper skirt of the passband is less steep than the lower skirt. This is often an undesirable phenomenon.

B.   TWO-PATH FILTERS

A better structure was proposed [Ref. 1] which eliminated most of the disadvantages of the first designs. It was a two path structure made by bifurcating a rectangular waveguide with a thin metal strip. This structure is shown in Fig. 2. The inherent advantages of this design include ease of manufacture and good reproduceability. Also, the resonant frequencies of either

4

Dielectric   Bifurcating metal plate

l_1 d_1 l_2 d_2 l_2 d_1 l_1

b a_1 t a_r

a

l_3 d_3 l_3
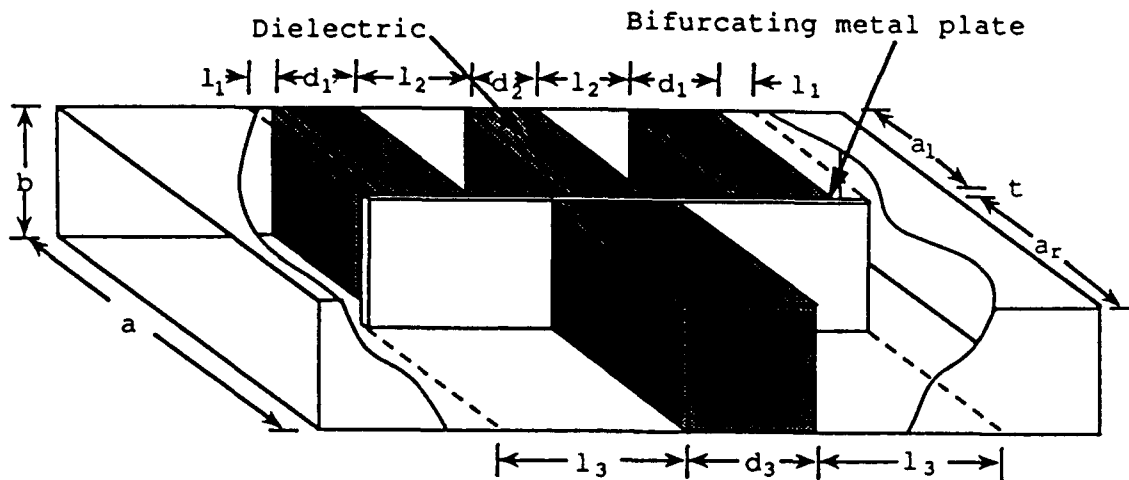
Figure 2. Two-path cutoff waveguide dielectric resonator filter

side of the bifurcated waveguide can be different from each other. The passband around the center frequency is set by the main path and is largely unaffected by the subsidiary path because the wave through that side is heavily attenuated by the cutoff nature of the bifurcated section around the passband frequencies. The resonant frequency of the subsidiary path can be higher than the passband set by the main path. The wave passing through that side at the subsidiary resonant frequency can be made equal in magnitude to that passing through the main path but 180° out of phase, hence the vector sum of both waves at that frequency is zero. This creates an attenuation pole which provides a steep skirt on the high frequency side of the passband. The chief advantage of this scheme is that the main path can be designed to meet a passband requirement, the subsidiary path

can be designed to meet a stopband requirement, and each path can be designed independently.

C. DESIGN PROCEDURES

The two-path structure described requires both a generalized scattering matrix technique and a less exact method using impedance converters. The structure is considered to be a direct-coupled cavity filter and is designed with a procedure based on that used by Levy [Ref. 4].

Because the subsidiary path has a negligible effect on the passband, it is replaced by a hypothetical infinitely long homogeneous below cutoff section in the design of the main path. The below cutoff sections in the main path are replaced by impedance inverters whose parameters, K and Φ, can be calculated from the T-equivalent circuit of a below cutoff section of waveguide of the appropriate length as shown in Fig. 3. The desired passband response then
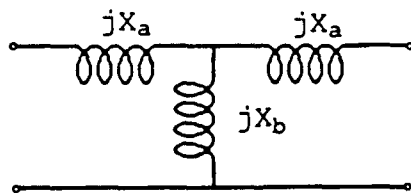
Figure 3. Symmetric T-equivalent circuit

determines the impedance inverters' parameters which determine X_a and X_b of the T-equivalent circuit which in turn give the necessary length of the below cutoff section.

6

The stopband response, however, requires the use of full
wave, multimode analysis. All sections in the bifurcated
waveguide are replaced by their generalized scattering
matrices which take into account several higher-order modes
as well as the fundamental mode. This is shown in Fig. 4.
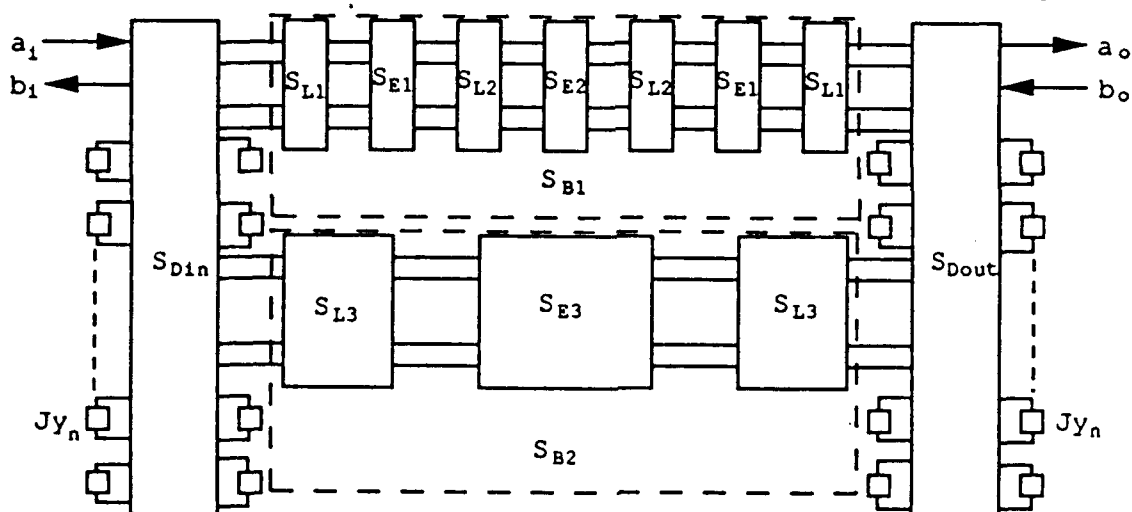
Figure 4. An equivalent circuit with generalized scattering matrices

The matrix element S_{21} of the overall scattering matrix of
the entire network can then be determined. It is a function
of the main path, which has already been specified, and the
length and ϵ_r of the dielectric block in the subsidiary
path. A CAD method was developed [Ref. 1] to determine the
length of the dielectric block given the desired minimum
loss in the stopband, the value of ϵ_r, and the main path
design.

The most apparent drawback of this method is that the T-
equivalent circuits modeling the first and last below cutoff
sections are not symmetric, as assumed. The discontinuity

caused by the edge of the bifurcating metal plate results in

an equivalent circuit shown in Fig. 5. The shunt reactance
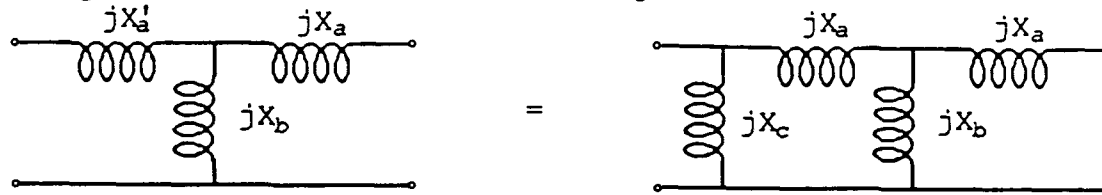
Figure 5.   Asymmetric *T*-equivalent circuit

element X_c must be canceled by another shunt reactance

element $-X_c$. This additional element is realized by a

capacitive window designed to provide the correct reactance

at the passband center frequency, f_o. Windows are placed

half a guided wavelength (at f_o) from both the input and

output discontinuity planes. Without the windows, passband

ripple would greatly exceed design requirements.

8

III. EQUIVALENT CIRCUIT MODEL

A. BASIC MODEL

The filter can be realized in the most rudimentary sense as a series of short rectangular waveguide sections with different values of relative permittivity. The height of each section in the model is the same as the height of the physical waveguide. The width of each section in the model is the same as the bifurcated section (the two sides are not
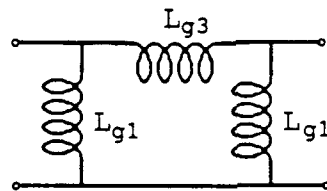
Figure 6. **Inductive Π-equivalent circuit of below-cutoff section**

necessarily identical). The below-cutoff sections may be replaced by their inductive Π-equivalent circuits as shown in Fig 6. The inductance values are given [Ref. 5] by

$$L_{g1} = L_{g2} = (X_o/2\pi f)\coth(\alpha T/2) \qquad (1)$$

$$L_{g3} = (X_o/2\pi f)\sinh(\alpha T) , \qquad (2)$$

where

$$X_o = 120\pi (2b/a) \sqrt{(f_c/f)^2 - 1}, \tag{3}$$

$$\alpha = (2\pi/\lambda) \sqrt{(f_c/f)^2 - 1}, \tag{4}$$

b, a, T are the height, width, and length of the below-cutoff section, and f_c is its cutoff frequency. These circuit elements are thus frequency-dependent. However, they can be computed analytically in a straightforward fashion. A disadvantage to using them is their frequency-dependence, which makes calculations necessary at each frequency point, which in turn makes simulation a slow and inefficient process. The thickness of the bifurcating metal strip is of little importance at this point. The lead section of one half λ_g at f_o is an air-filled length of standard rectangular waveguide.

The reactance elements realized by symmetric capacitive windows are incorporated in the model as frequency-dependent capacitors. The value of these elements is given [Ref. 6: pp. 314-315] by

$$\frac{B_c}{Y_o} = \frac{4b}{\lambda_g} \ln (\csc (\frac{\pi d}{2b})), \tag{5}$$

where B_c is the susceptance, Y_o is the characteristic admittance, b is the height of the rectangular waveguide, and d is the size of the window as shown in Fig. 7. In the

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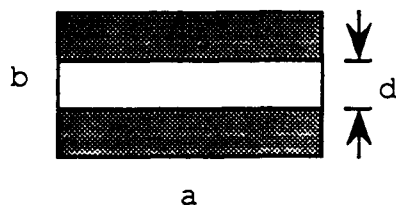
Figure 7. Capacitive window

computer model, the normalized susceptance must be converted
to a value of capacitance by dividing it by $2\pi f Z_0$ where the
characteristic impedance is frequency-dependent .

The discontinuity of the thin bifurcating metal plate is
the most challenging part of the model. It is also very
critical. Previous studies of a thin metal septum in
waveguide [Ref. 5] suggest that the discontinuity is most
simply modeled by a single, frequency-dependent inductor.
For better accuracy, it can be modeled using a fixed
inductor in parallel with a fixed capacitor.

When all the pieces are finally brought together, the
entire model appears as shown in Fig. 8.

B. A SPECIFIC EXAMPLE

The first device to be modeled was a filter described by
Shigesawa *et al*. [Ref. 2]. This particular device was
chosen because the design specifications and parameters were
given along with experimental results. The filter design
specifications are given in Table 1, the filter parameters
are given in Table 2, and the measured insertion loss is
shown in Fig. 9. The residual insertion loss of about 0.5

11
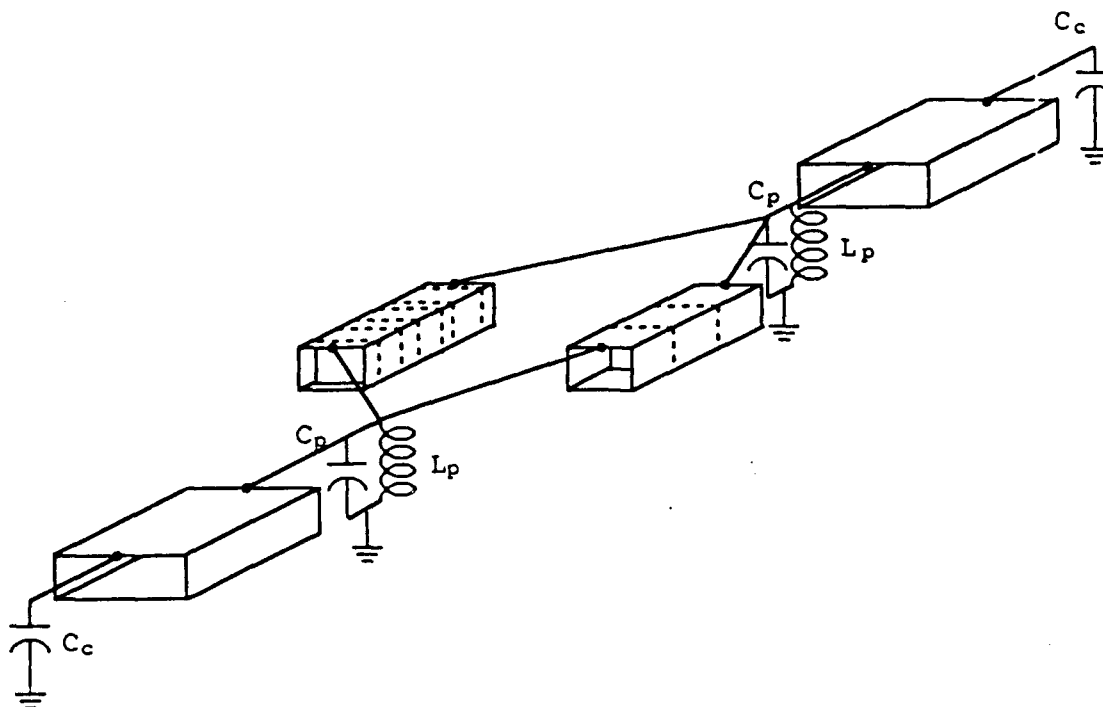
Figure 8. Basic circuit model of the two-path filter

dB in the passband is attributed to gaps between the

dielectric blocks and the waveguide walls.

TABLE 1. DESIGN SPECIFICATIONS

Passband response	3-poles, 0.1 dB Chebyshev
Center frequency	f_o = 9.5 GHz
Bandwidth	Δf = 0.3 GHz
Fixed attenuation pole or stopband edge	$f_{\infty 1}$ or f_{s1} = 11.0 GHz
Minimum insertion loss in the stopband	L_{min} = 50 dB

TABLE 2.   DESIGN PARAMETERS

Parameter	Length (cm)
a_l	1.18
a_r	1.09
l_1	0.69
l_2	1.33
l_3	2.01
d_1	0.40
d_2	0.40
d_3	1.22
ϵ_r	3.78
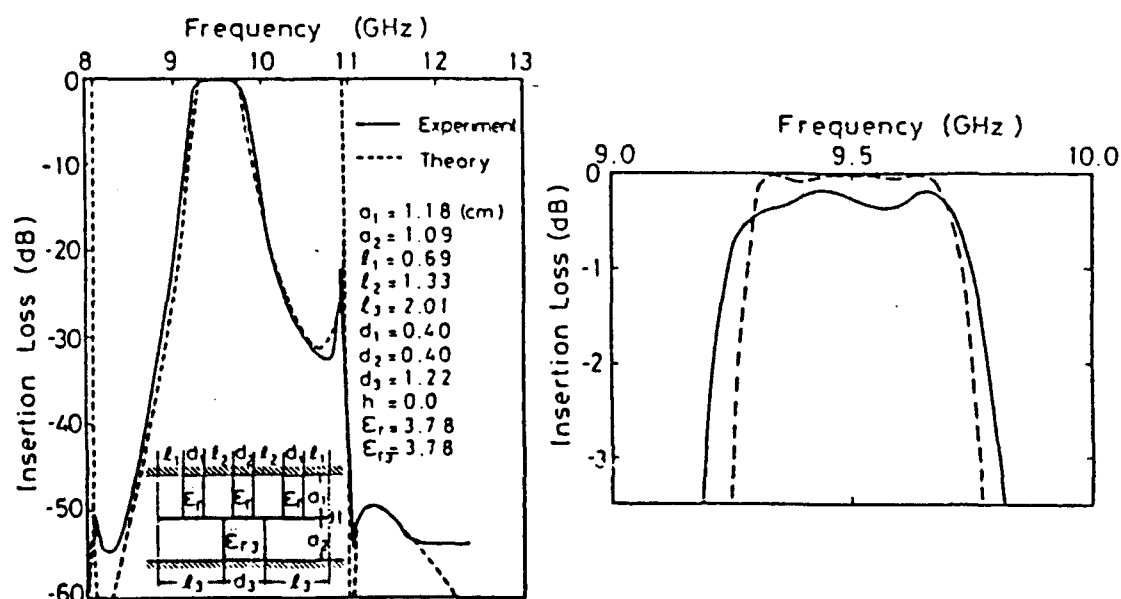
Figure 9.   Measured response of the filter

The *Touchstone* circuit file incorporating the model is included as Appendix A.   The model is the same as that shown in Fig. 8, with the parameters set to the values given in Table 2.   Input and output ports are terminated in a matched

13

load (RWGT). The capacitive windows are modeled as described previously (Eq. 5). The one-half guided wavelength at f_0 is incorporated not as a fixed length, but as a function of f_0 itself. This does not significantly affect the time of a frequency sweep as the calculation is done only once.

The results of sweeping this model are shown in Fig. 10. and Fig. 11. A comparison of these figures to Fig. 9 indicates the gross features of the experimental frequency response are simulated well by the model. These include the resonance at 8.1 GHz and the attenuation pole at 11.0 GHz.
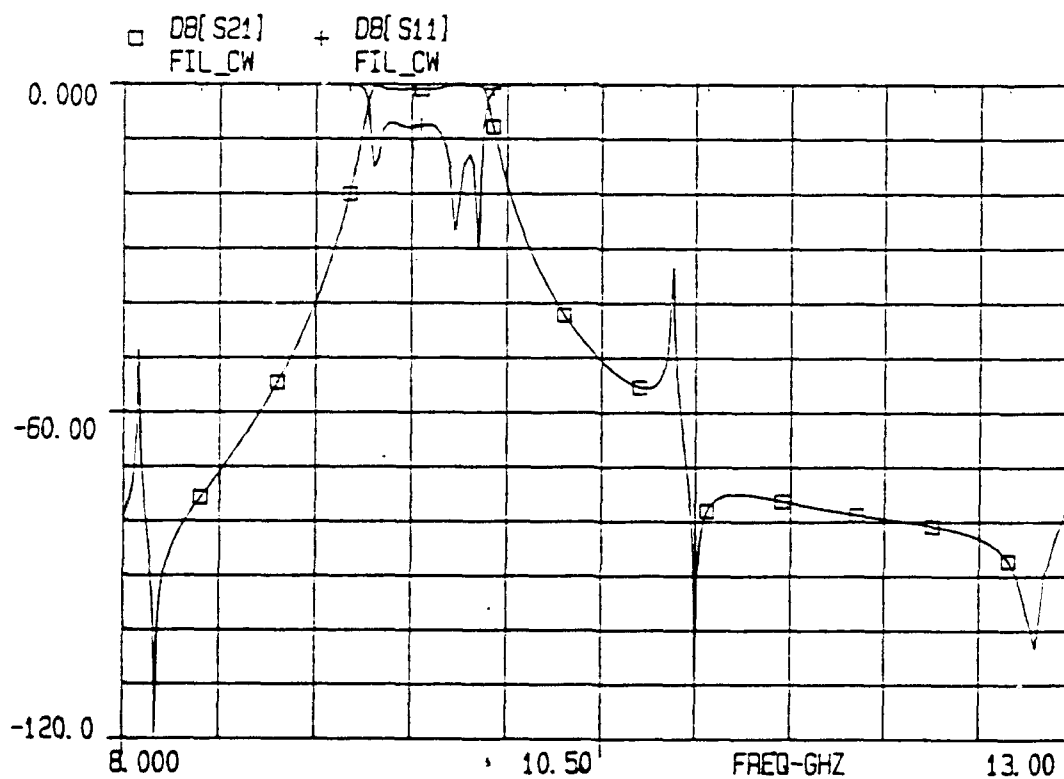
Figure 10.   Frequency response of the basic model
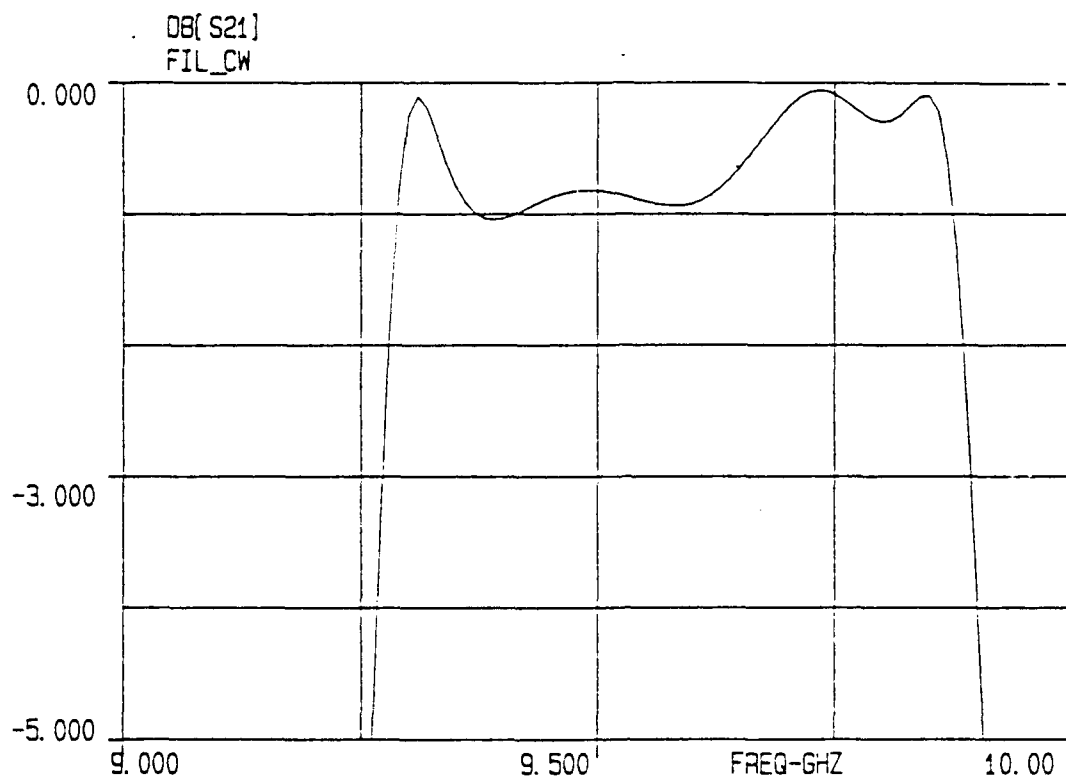
Figure 11. Frequency response of the basic model

However, the exact characteristics of the passband are less than satisfactory.

C. IMPROVEMENT TO *E*-PLANE DISCONTINUITY MODEL

Analysis of Fig. 11 indicates that the passband ripple is 1.1 dB when a ripple of 0.5 dB was expected. Although the performance specifications called for a 0.1 dB ripple, the goal was to match the performance of the physical device, so the model's performance must be compared to the experimental results.

It was determined that the best modification to the model was to change the discontinuity elements from a single

15

parallel inductor and capacitor to a pair of parallel inductors and capacitors. That is, a different inductor and capacitor value would be associated with the main path and the subsidiary path. This modification can be seen in Fig. 12. The reasoning behind this configuration is that the presence of the dielectric block in the below cutoff section has an affect on the discontinuity element values. Instead of being 14.0 nH in parallel with 0.003 pF as in the case of
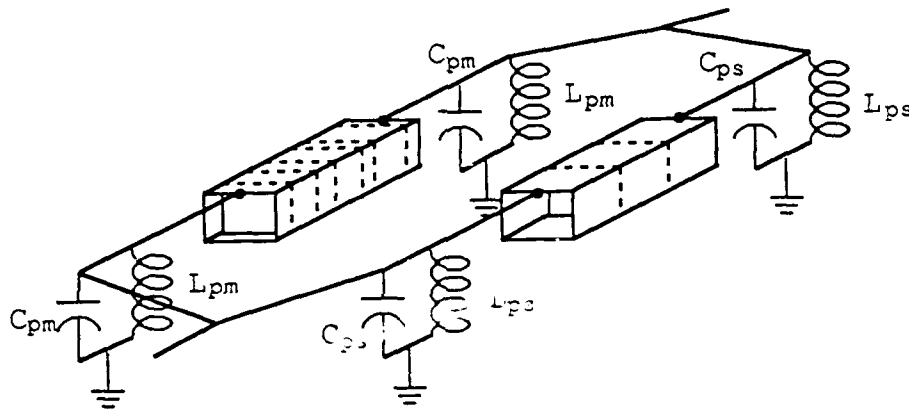
Figure 12. **Modification to the model**

a long section of air-filled bifurcated waveguide, they would be different.

1. Investigation of bifurcated waveguide with a dielectric block

The problem, of course, was to determine the values of the new elements. To this end, a long section of bifurcated waveguide with a small dielectric block was constructed in the lab as shown in Fig. 13. The scattering parameter S_{11}

16

was measured at every 500 MHz from 8.0 GHz to 12.0 GHz.
Also, several sweeps were made. Each time, the distance, L,
from the discontinuity plane and the leading edge of the
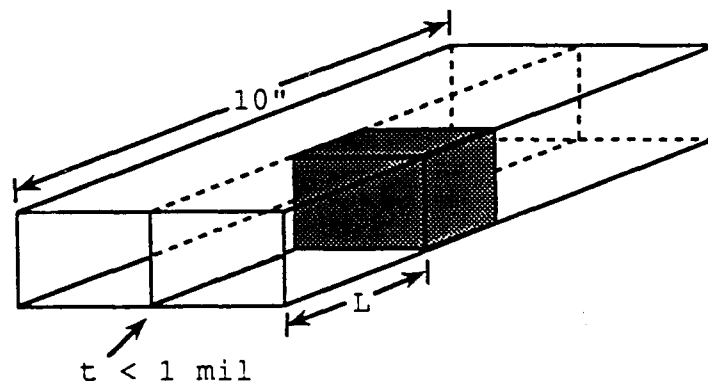
Figure 13.   Bifurcated WG with dielectric block

dielectric block was increased. The lengths used were 100,
150, 200, 250, and 300 mils. The data was collected at each
point via a slotted line and a VSWR meter. It consisted of
the distance between a null with a short and a null with the
bifurcated waveguide. It also included the difference in
magnitude between adjacent VSWR minima and maxima. The
final results of this experiment, represented as angle and
magnitude of S_{11} at each frequency, are included as Appendix
B.

2. Matching the experimental data

To determine the discontinuity element values, the
experimental set up was modeled in a *Touchstone* file
included as Appendix C. This file incorporates the
discontinuity elements as a different pair of parallel

inductors and capacitors like that shown in Fig. 12 above.
The elements associated with the section with no dielectric
block were given the proven values of 14.0 nH and 0.003 pF.
The optimizers available in *Touchstone* were used to
determine the values associated with the dielectric-loaded
section which resulted in the best agreement between
experimental data and that produced by the model. The
results are shown in Table 3.

TABLE 3. DISCONTINUITY ELEMENT VALUES

L (mils)	L_{pm} (nH)	C_{pm} (pF)
300	15.21	0.001
250	16.55	0.00025
200	18.60	0.00019

Unfortunately, *Touchstone* exhibits some anomalous
behavior when very short rectangular waveguide sections are
used. That is, at $L \approx 190$ mils, the frequency response was no
longer as well behaved or predictable as it was with longer
sections. This means that discontinuity element values for
$L = 150$ mils and $L = 100$ mils were not found.

D. FINAL MODEL

Once the proper discontinuity elements had been found,
they were incorporated in the model. The *Touchstone* circuit

file incorporating this modification is included as Appendix

D. It is still based on the design reported in Ref. 2.

The frequency response of this model is shown in Fig. 14

and Fig. 15. Although the ripple in the passband is 0.8 dB,

it is far better than that given by any other configuration.

Also, the position of the attenuation pole at 11.0 GHz as

well as the lower-order mode subsidiary path resonance at

8.1 GHz are positioned exactly as reported by Shigesawa *et*

al.
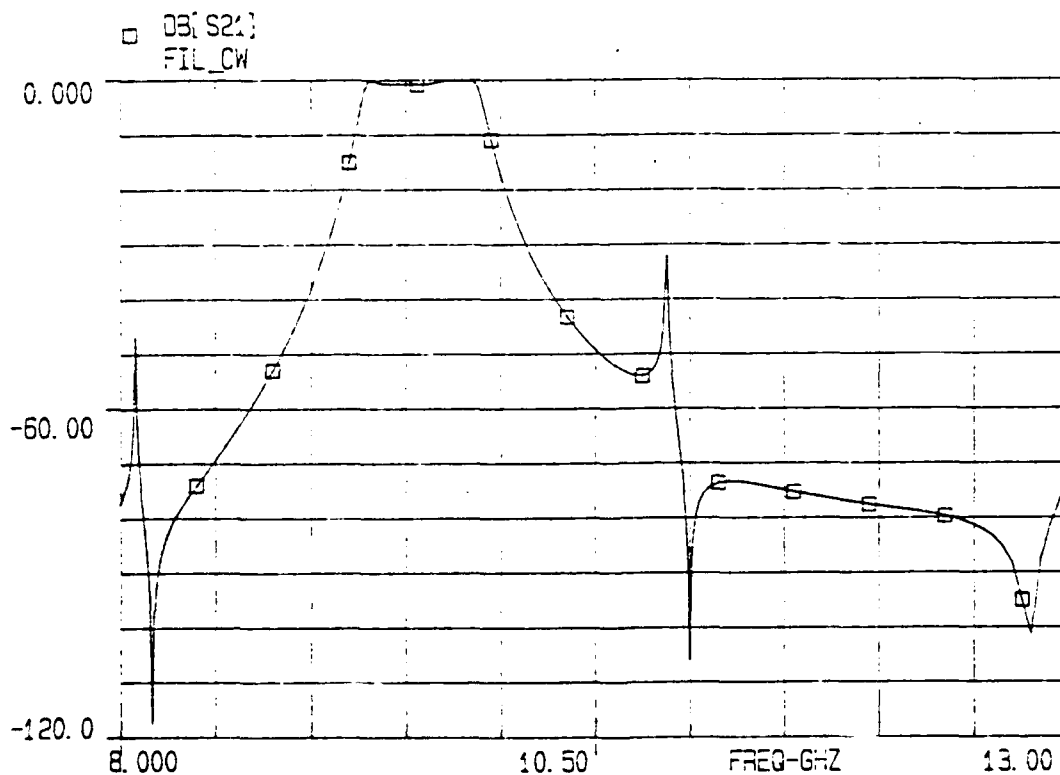
Figure 14. Frequency response of the final model
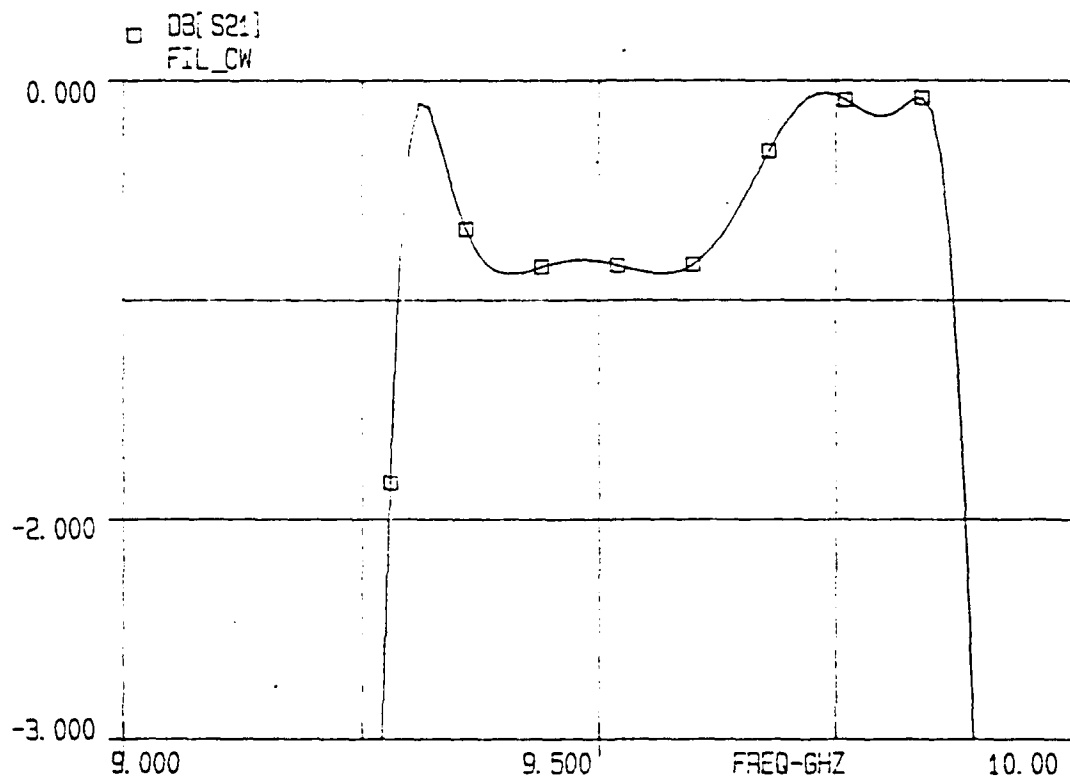
Figure 15. Frequency response of the final model

IV. A DESIGN PROCEDURE

A. SELECTING THE OPTIMIZER

The optimizer resident in *Touchstone* uses one of three search procedures in conjunction with one of four cost functions [Ref. 7]. Choosing the correct search procedure and the correct cost function to be minimized are vital to obtaining a reasonable design in a short period of time.

It was decided to start the search using the Random Search procedure in which new values for the user-specified parameters are selected by a random number generator. Although a random search may appear inefficient, it is faster than the Gradient Search which chooses values according to the gradient of the cost function (it always moves in the direction of decreasing cost). Once the Random Search produces parameter values nearing a solution as indicated by a slowly decreasing cost function, the Gradient Search was used to further refine the design. Thus, the best solution is found in the shortest time. The third search method, Quasi-Newton, was not used because a single iteration required a much longer time than was deemed reasonable.

Selecting the appropriate cost function was less difficult. The Minimax Cost Function leads to a solution in

21

which the point of maximum error is minimized. That is, it leads to an equal ripple solution. This would appear to be the ideal selection as the design will ultimately resemble a Chebyshev response. However, Minimax (as well as the Least P^{th} cost function) are very limited in the number of frequency points allowed, which makes them unusable for such a complicated problem. The third cost function, known as Worst-case, is used to negate the error function, thereby allowing one to find the worst instead of the best solution. Although useful for a worst case analysis of a circuit, it is inappropriate for a design procedure. The last cost function is the Least Squares Cost Function. In it, the squared error between actual response and desired response at each frequency is minimized. This cost function was chosen because of its simplicity and the fact that the other cost functions had been eliminated.

B. DESIGN PROCEDURE

The actual values of the individual elements of the device will be found by the optimizer (Random then Gradient search procedures using the Least Squares error function). Many parameters will have to be selected for the optimizer to function correctly. That is, almost the entire circuit file must be set up leaving only a few parameters to be found. First, the size of the waveguide to be used including the dimensions of the main and subsidiary path

must be chosen. Of course, the value of the dielectric's relative permittivity, ϵ_r, must be chosen based on available materials. Because the values of the discontinuity elements depend on the distance between the first dielectric block and the edge of the bifurcating metal septum, the value of l_1 (in Fig. 2) must be fixed along with the associated discontinuity elements. Once the circuit file has been created with the appropriate values, the optimizer will find the values of d_1, d_2, d_3, l_2, l_3, and d (the size of the capacitive window).

The entire filter cannot be designed at once. Separation of the main and subsidiary paths is necessary. The main path which determines the passband characteristics must be designed first and then the subsidiary path must be determined. First, the subsidiary path is replaced by a long section of below-cutoff waveguide. The length depends on the size of the guide. For example, 7 cm is l⟨ ⟩ enough for standard WR-90. The discontinuity elements associated with the subsidiary path must remain in place. Given a reasonable goal, such as FIL_CW DB[S21] > -0.1 in the OPT block of the circuit file, the optimizer will find the best values of l_2, d_1, d_2, and d. Once these numbers are set, the subsidiary path will be replaced. To ensure the subsidiary path will be the same length as the main path, the lines

L_TOT=2*(L1+L2+D1)+D2
L3=(L_TOT-D3)/2

23

must be included in the EQN block. Thus, d_3, the length of the dielectric block in the subsidiary path, can be varied alone while keeping the total length of the subsidiary path equal to that of the main path. The subsidiary path is designed only to provide an attenuation pole on the high frequency side of the passband. Because the location of a pole cannot be specified explicitly in the OPT block, the TUNE command will be used to vary d_3 manually until the pole of the entire model (both main and subsidiary paths at this point) appears at the desired position. Although such a "trial and error" method lacks elegance, it is an efficient way to fix the location of the attenuation pole, and clearly illustrates the power of computer-aided design.

Separation of the two paths *for design purposes* is allowed [Ref. 2] because the subsidiary path has a negligible effect on the passband response. A *Touchstone* circuit file exploring this assumption is included as Appendix E. The model parameters are the same as those already given (Table 2). The results of separating the two paths in this file are shown in Fig. 16 and Fig. 17. Comparison of Figs. 14 and 16 reveals that the separation of the two paths is valid. The passband remains essentially unchanged. The high frequency attenuation pole is realized from the outputs of the paths being equal in magnitude (-62 dB) and 180° out of phase (a phase angle of -35° for the

24
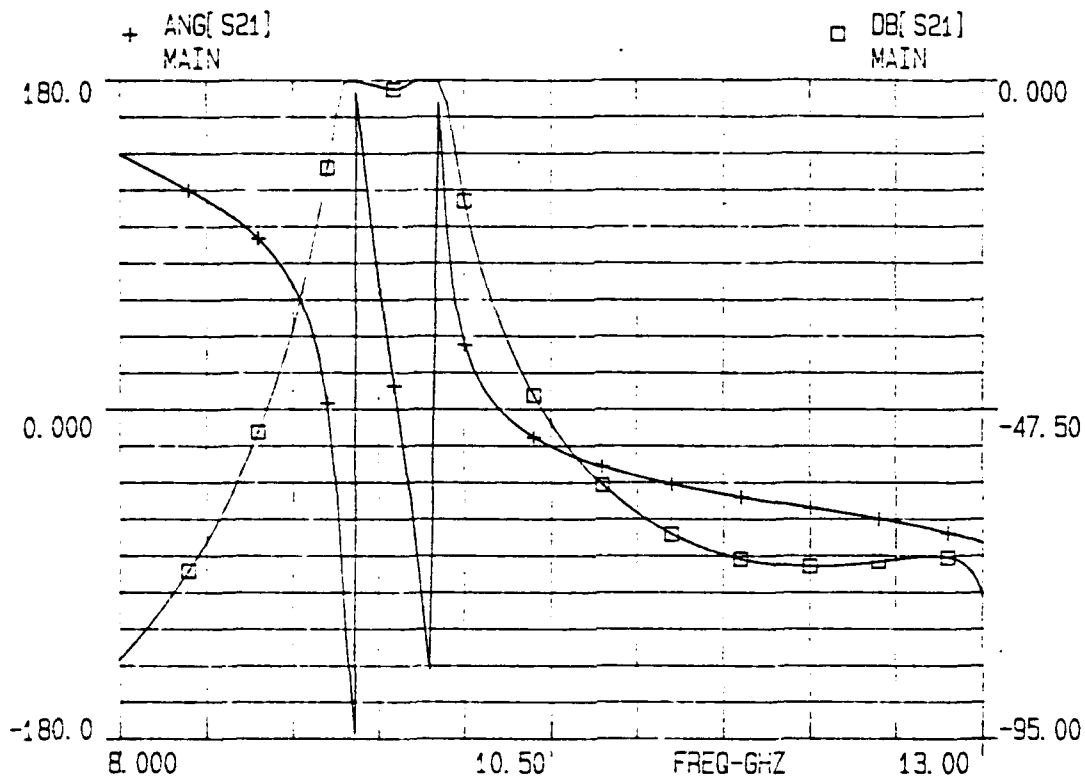
Figure 16. Frequency response of main path
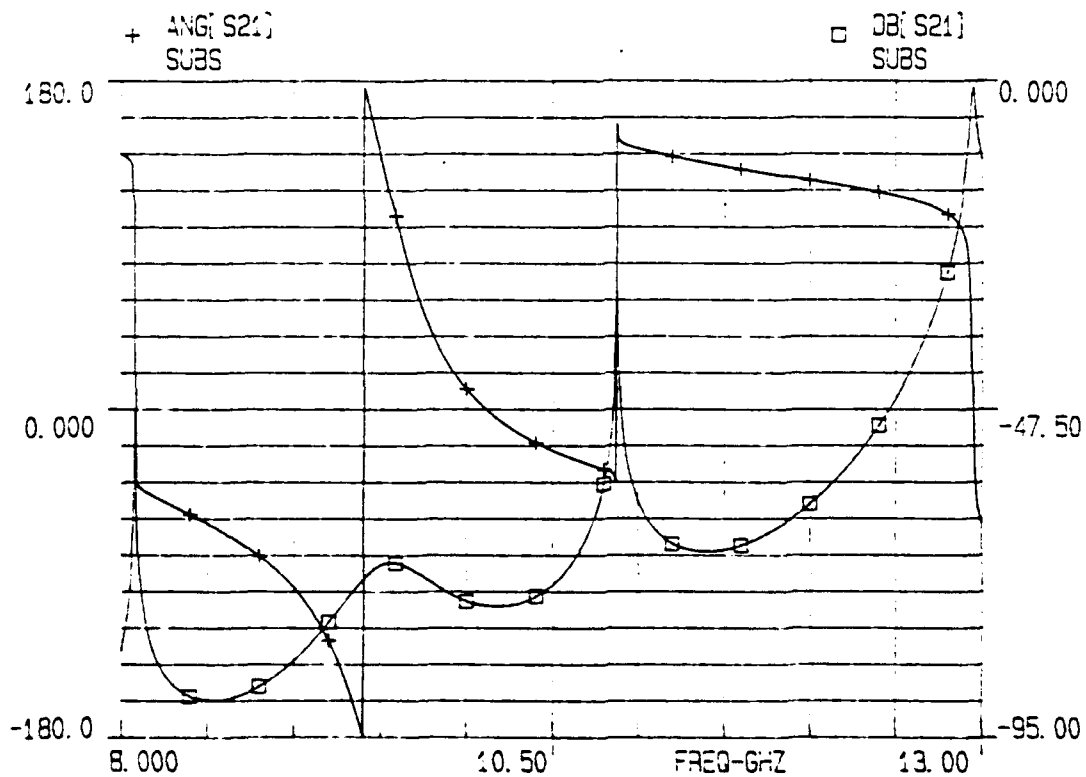
Figure 17. Frequency response of subsidiary path

25

main path and 145° for the subsidiary path), as discussed earlier.

Initial values for d_1 and d_2 are set by the desired center frequency of the passband. The TE_{mnp} resonant frequency, f_r, of a perfect rectangular cavity is given by the equation [Ref. 6: pp. 430-439]:

$$f_r = \frac{c}{\sqrt{\mu_r \epsilon_r}} \sqrt{(\frac{m}{2a})^2 + (\frac{n}{2b})^2 + (\frac{p}{2d})^2}, \qquad (6)$$

where a, b, and d are the dimensions of the rectangular cavity. Solving for d in the TE_{10p} mode results in

$$d = \frac{p}{2\sqrt{\frac{f_r^2 \mu_r \epsilon_r}{c^2} - (\frac{1}{2a})^2}}. \qquad (7)$$

The variable d gives the value of d_1 or d_2. Since this equation applies to a perfect cavity, the resonant frequency, f_r, must be set well above the desired frequency. Experience indicates a value 1.8 times greater than that desired will be appropriate. In order for this assumption to remain valid, the coupling into the cavity must be similar to that for which the above rule of thumb was formed. Therefore the initial value of l_2 will be set. The initial value for d_3 can be found using the same equation. In all cases, the TE_{101} mode as well as the TE_{102} mode should be considered.

C. A DESIGN EXAMPLE

Using the procedure described above, a design example was pursued. The design specifications are given in Table 4. Because the dielectric material to be used had a

TABLE 4. DESIGN SPECIFICATIONS

Passband response	3 poles, 0.1 dB Chebyshev
Center frequency	f_o = 10.5 GHz
Bandwidth	Δf = 0.3 GHz
Fixed attenuation pole or stopband edge	$f_{\infty 1}$ or f_{s1} = 12.0 GHz
Minimum insertion loss in the stopband	L_{min} = 35 dB

relative permittivity of 2.54, the center frequency could not be lower than 8.5 GHz because the bifurcated section filled with the dielectric material had a cutoff frequency of 8.23 GHz. The rest of the design specifications are similar to those found in Ref. 2.

The fixed values are summarized in Table 5. To ease fabrication, a standard WR-90 waveguide was split in equal halves, so both the main path and the subsidiary path would be the same width. Also, as mentioned above, the only useable dielectric material available was Poly-C with ϵ_r = 2.54. The value of l_1 was set at 300 mils (0.762 cm) because the discontinuity elements associated with that

TABLE 5. FIXED DESIGN PARAMETERS

Parameter	Value
a_l	1.143 cm
a_r	1.143 cm
ϵ_r	2.54
l_1	0.762 cm (300 mils)
L_{pm}	15.21 nH
C_{pm}	0.001 pF

length matched the experimental data gathered earlier
slightly better than the other possible choices.

The initial and final values of the optimized parameters
are given in Table 6. The *Touchstone* circuit file

TABLE 6. OPTIMIZED PARAMETERS

Parameter	Initial value (cm)	Final value (cm)
l_2	1.00	1.50883
d_1	0.60	0.63037
d_2	0.60	0.60423
d	0.1016	0.14934
d_3	1.22	1.740
l_3	N/A	2.333

incorporating this design is included as Appendix F. The
optimization of the main path was accomplished with the
statements

28

```
RANGE 10.35 10.65
FIL_CW DB[S21] > -0.1
```

in the OPT block of the file. The frequency response of the

final design is shown in Fig. 18 and Fig. 19. Although the

design specifications called for a passband ripple of 0.1

dB, a ripple of 0.2 dB was deemed acceptable in part because

the difference between 0.1 dB and 0.2 dB is a difference of

less than 2.2 %. The response of the main path alone is

shown in Fig. 20 to illustrate the effectiveness of the

subsidiary path in increasing the steepness of the upper

frequency skirt of the passband.
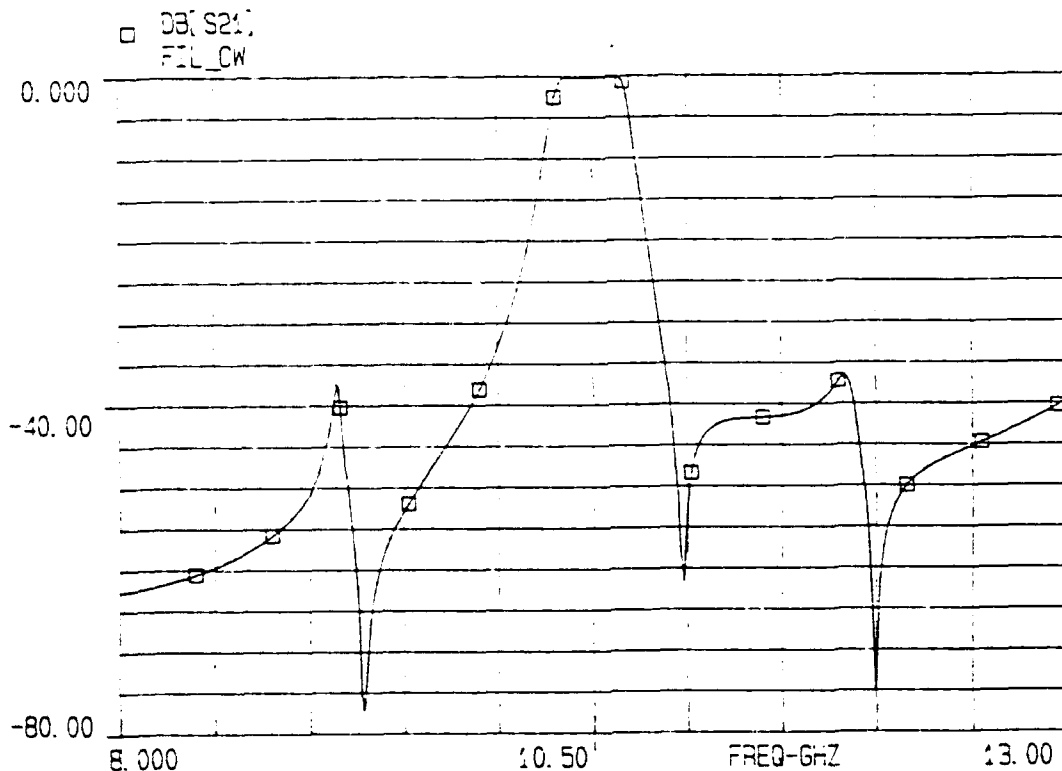
Figure 18. Frequency response of the designed model
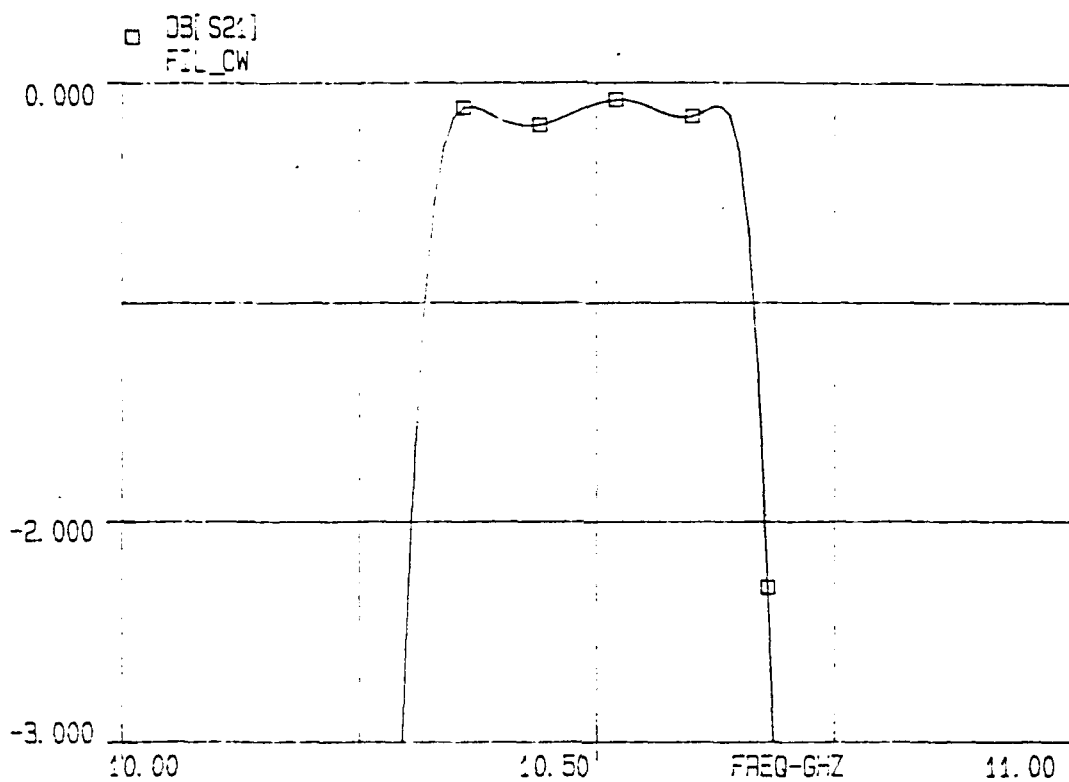
Figure 19. Frequency response of the designed model
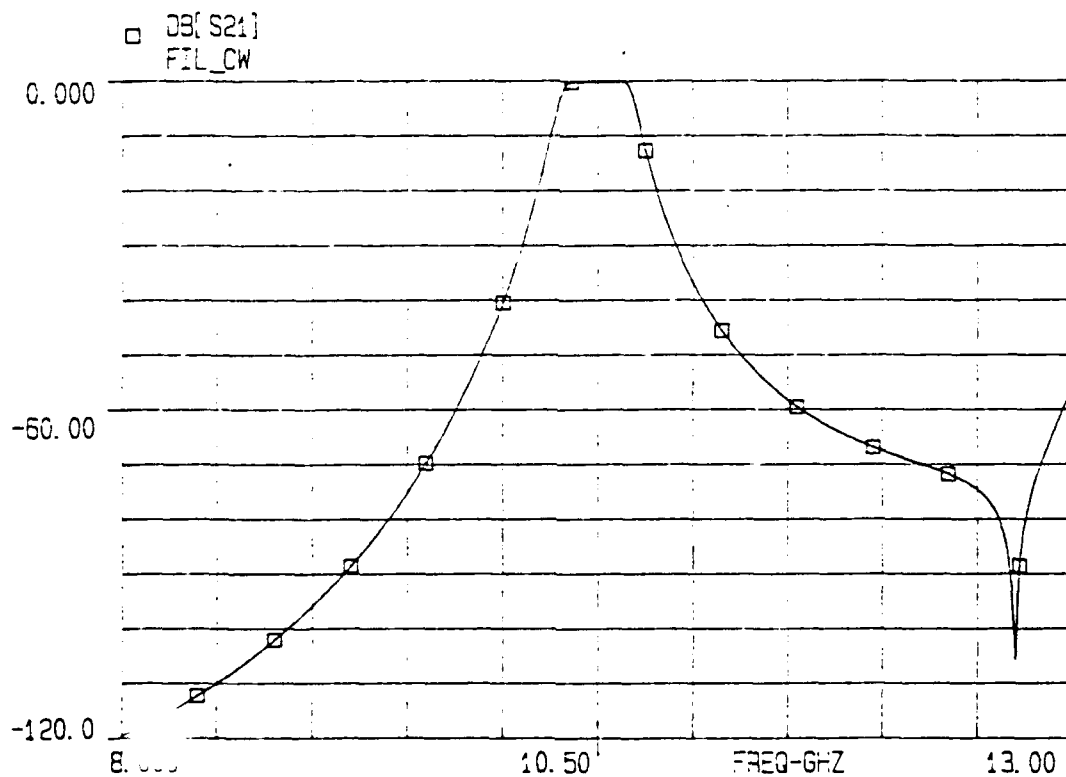
Figure 20. Frequency response of the main path

30

D. EXPERIMENTAL PERFORMANCE OF DESIGNED FILTER

The above filter was fabricated in accordance with the above specified parameters. Photographs of the filter are shown in Fig. 21 and Fig. 22. The filter itself was manufactured from aluminum barstock with internal dimensions equivalent to those of standard WR-90 rectangular waveguide. The capacitive windows were cut from a copper sheet 0.05 cm thick. The bifurcating metal septum was cut from copper foil 0.005 cm thick. Because of limitations in the machining process, some measurements were different from those specified. Table 7 summarizes the actual measured dimensions.

TABLE 7. PARAMETERS OF MANUFACTURED FILTER

Parameter	Length (cm)
d_1	0.630
d_2	0.600
d_3	1.740
L_c	1.835
d	0.1491
l_1	0.762
l_2	1.509
l_3	2.330

The frequency response of the filter was measured using an HP 8756A Scalar Network Analyzer. The "through"

31
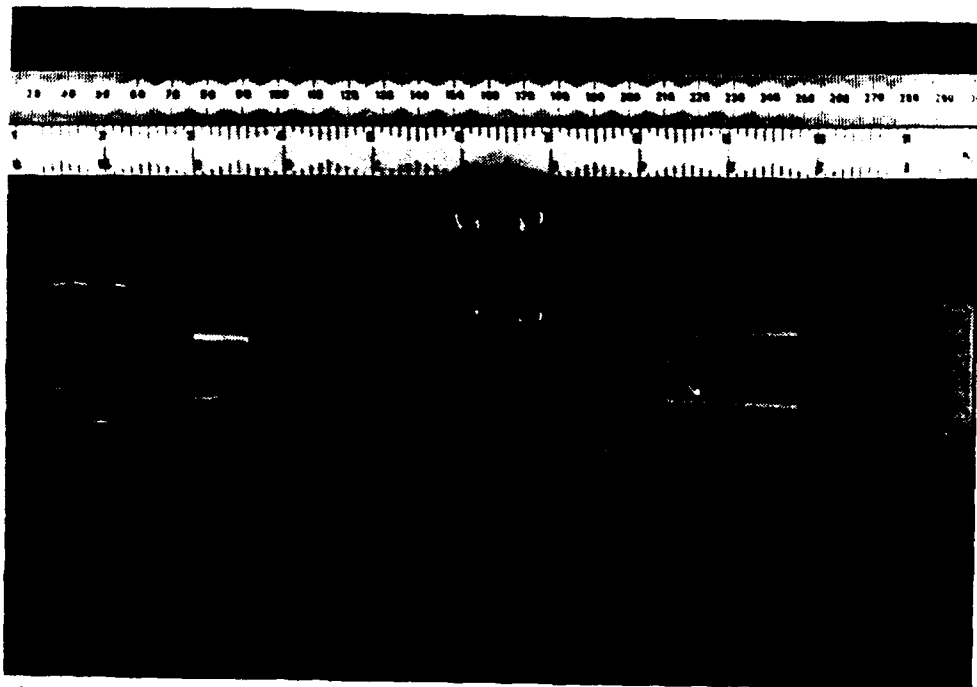
Figure 21. Photograph of disassembled filter
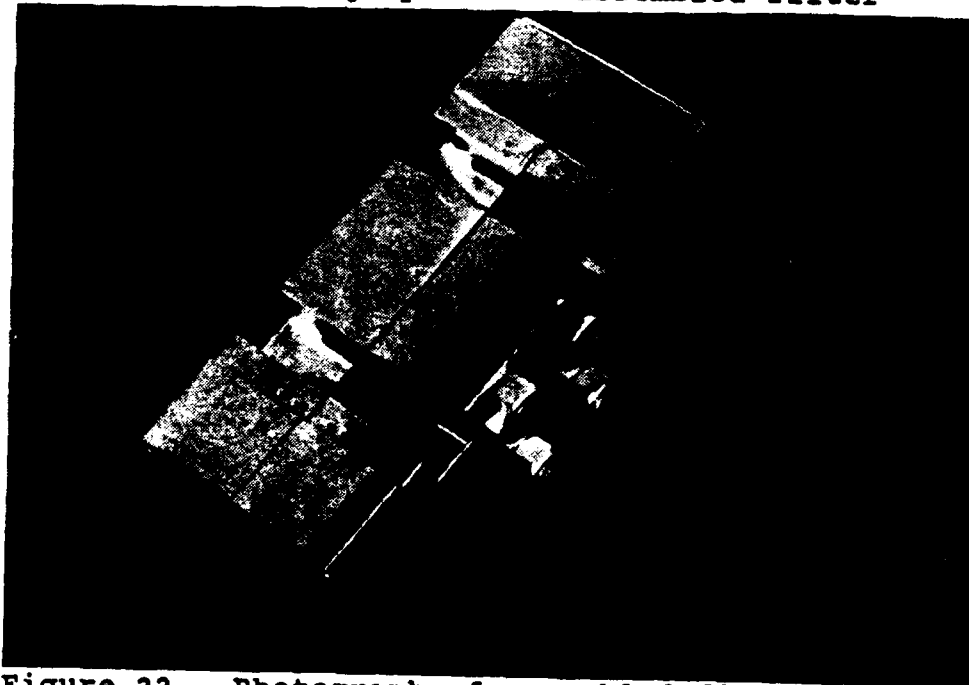
Figure 22. Photograph of assembled filter

calibration was accomplished by placing the filter assembled
without the dielectric blocks and without the metal septum

between the test ports. This was done to remove losses due to the various connectors and adapters from the final results. The frequency response of the filter is shown in Fig. 23 and Fig. 24. The response is very similar to that predicted by the model. The response of the model incorporating the actual measurements is shown in Fig. 25 and Fig. 26. One can see that the gross features of the filter's frequency response were predicted by the model. These include the resonance at about 9.2 GHz and the position and magnitude of the first ripple of the passband. The discrepancies between tne model response and the actual response are due to transmission loss, gaps between the waveguide walls and the dielectric blocks, misalignment of the capacitive windows, misalignment between adjacent waveguide sections, misalignment of the two halves of the split sections, and problems with the metal septum which include bends of the septum within the body of the filter, overlap and non-vertical alignment at either end leading to a severe folding of the septum itself.

REF 2

STRT +8.0000GHz   STOP +13.0000GHz
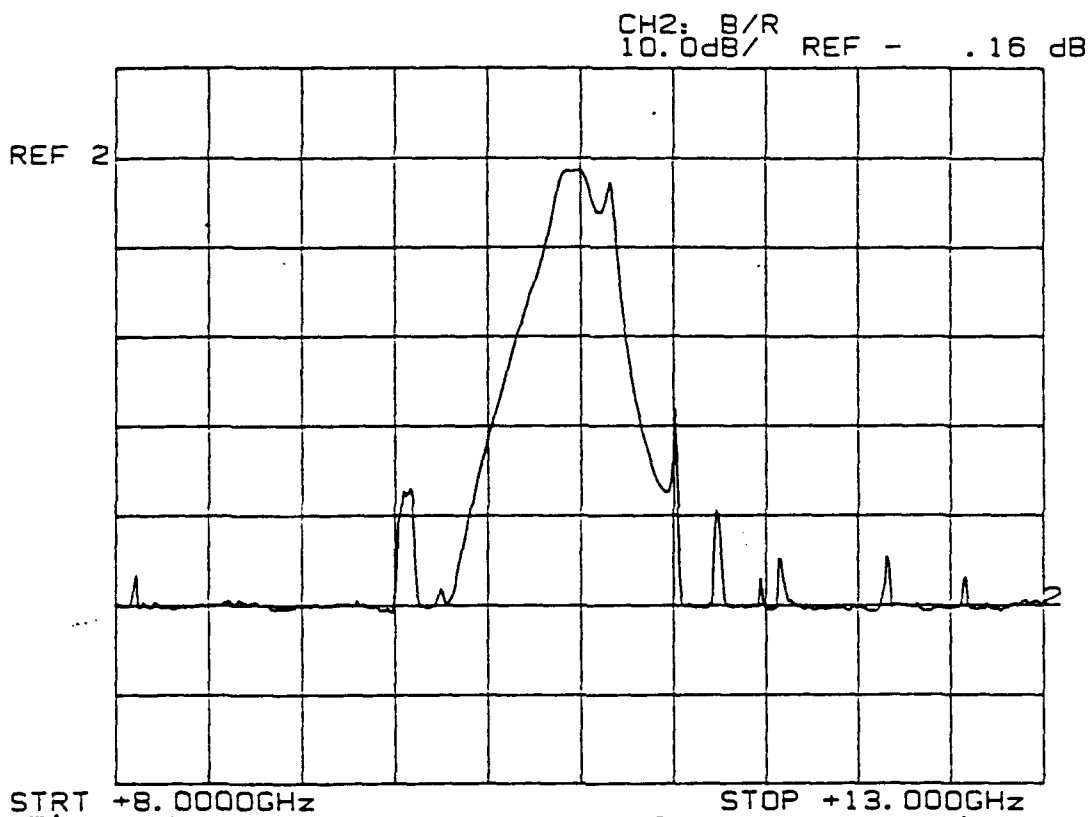
Figure 23.   Frequency response of manufactured filter

REF 2

STRT +10.000GHz   STOP +11.000GHz
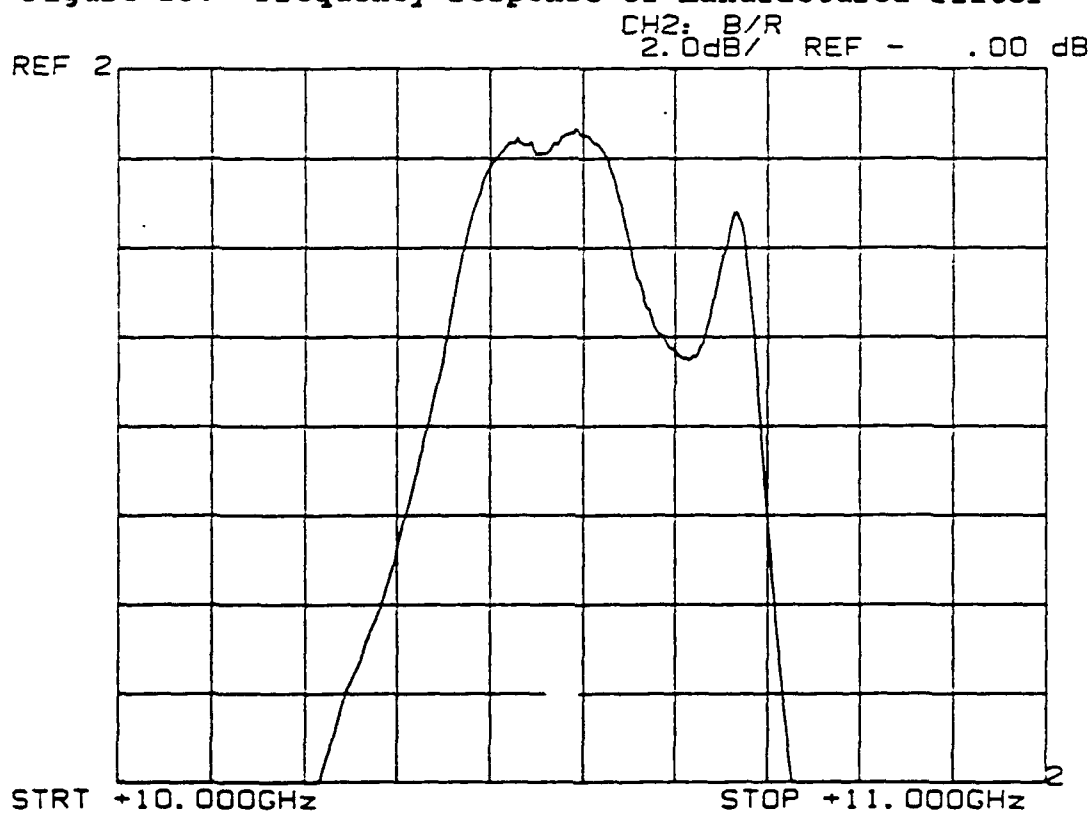
Figure 24.   Frequency response of manufactured filter

34
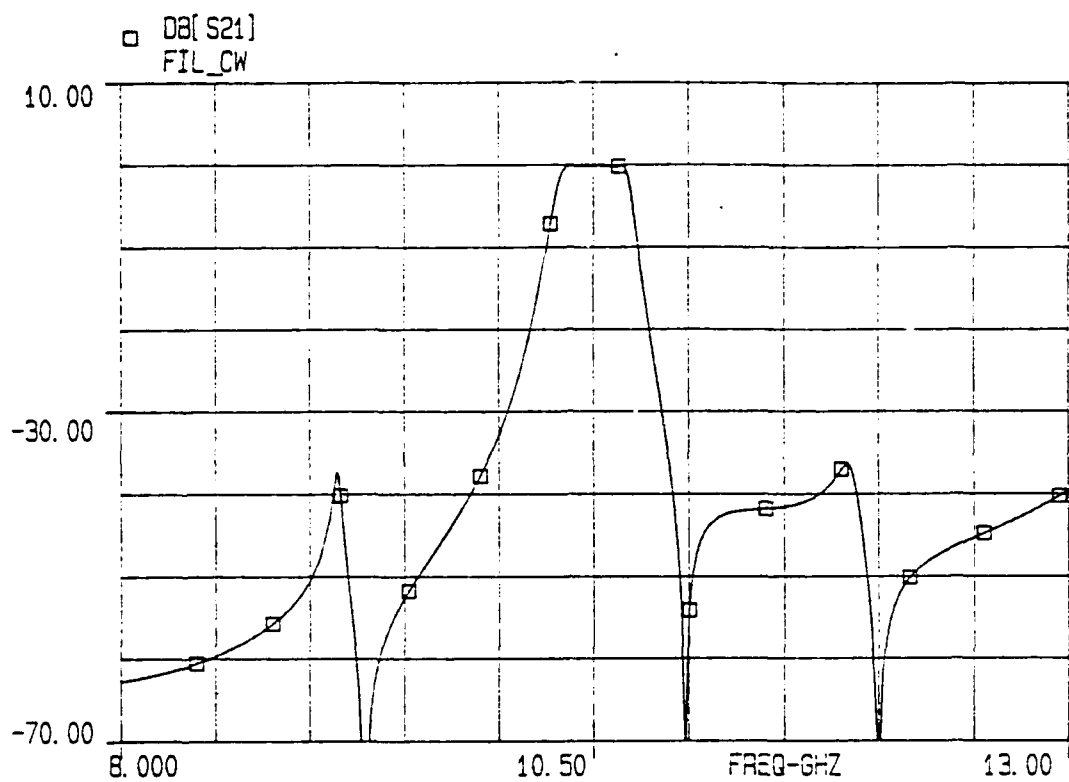
Figure 25. Frequency response of model as manufactured
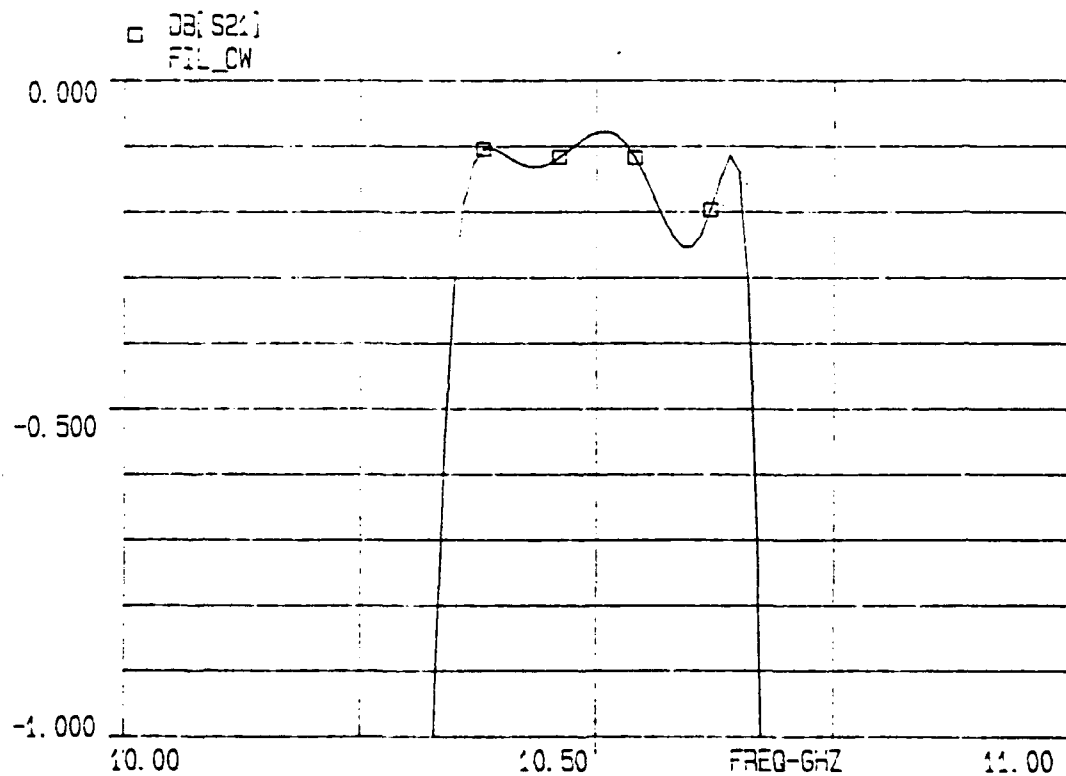
Figure 26. Frequency response of model as manufactured

35

V. CONCLUSIONS AND RECOMMENDATIONS

A. CONCLUSIONS

This thesis has shown that a two-path cutoff waveguide dielectric resonator filter can be accurately modeled by a simple equivalent circuit using available library elements in a commercial CAD system. Such a model was developed and its performance was shown to match that of an actual device very closely. The positions of the attenuation poles were placed exactly, and the passband ripple was matched to within 0.3 dB.

The circuit model was then used to successfully design this type of filter to prescribed performance criteria using optimizer algorithms. This design approach proved faster and more accurate than design procedures used previously.

B. RECOMMENDATIONS FOR FURTHER STUDY

The effect of the dielectric blocks on the discontinuity element values requires more study in order to develop a complete list matching the distance between the edge of the metal septum and the first dielectric block with the appropriate discontinuity element values. Strategies other than adding discrete elements should also be thoroughly investigated.

The ultimate goal should be to further automate the design process, allowing a user with little or no experience with these filters to effectively design a filter to meet any specifications.

APPENDIX A.   BASIC MODEL *TOUCHSTONE* CIRCUIT FILE

```
! FILE:      Two-Path Dielectric Resonator Filter (TPDRF)
! USER:      LT Gregory Miller
! DATE:      24 SEP 91
! REVISED:   3 OCT 91
! CIRCUIT:   Two-path cutoff waveguide dielecrtic resonator
!      filter

! COMMENT:   This file is a trial of some different WG/dielectric
!      combinations.  It is based on a design in Ref.2
!
!      It simulates both halves of a split WG, with a parallel
!      inductor and capacitor to model the losses due to the
!      dicontinuity between the standard WG and the split
!      section.
!
!      It also incorporates the capacitive window absent from
!      previous programs.  It is implemented as a
!      frequency-dependent capacitor.  The frequency dependence
!      is represented as an equation  relating Bc/Yo to
!      capacitive window geometry found in Ref. 6.


DIM
   FREQ GHZ
   RES OH
   IND NH
   CAP PF
   LNG CM
   TIME PS
   COND /OH
   ANG RAD


VAR
   Ag=2.286 ! WR-90 WG
   Al=1.18  ! Left and right halves are not symmetric
   Ar=1.09
   B=1.016

   ER=3.78  ! Dielectric constant used by Shigesawa, et al.

   L1=0.69  ! Length of 1st & last air-filled section, main path
   L2=1.33  ! Length of 2nd & 3rd air-filled section, main path
   L3=2.01  ! Length of 1st & last air-filled section, subs path
   D1=0.40  ! Length of 1st & last er-filled section, main path
   D2=0.40  ! Length of middle er-filled section, main path
   D3=1.22  ! Length of er-filled section, subsidiary path
```

```
      Cp=0.006 ! Value of parallel capacitor (pF)
      Lp=7.0   ! Value of parallel inductor (nH)
      d=0.1138 ! Size of capacitive window (cm)


   EQN
   ! Equations for FREQ-dependent element (capacitive window)
      PI=3.1415927
      Fc=6.562                       ! Cutoff frequency
      Fo=9.5                         ! Center frequency
      lam=30/FREQ                    ! Wavelength in cm if FREQ in GHz
      Gfac=(1-(Fc/FREQ)**2)**0.5     ! Guide factor
      lamg=lam/Gfac                  ! Guided wavelength
      Zo=(120*PI*2*B/Ag)/Gfac        ! Characteristic impedance
      Bc_Yo=(4*B/lamg)*LN(1/SIN(PI*d/(2*b)))! Normalized susceptance
      Cc=1000*Bc_Yo/(Zo*2*PI*FREQ)   ! FREQ-dependent capacitance
      Gfaco=(1-(Fc/Fo)**2)**0.5      ! Guide factor at Fo
      Lc=0.5*(30/Fo)/Gfaco           ! Half a guided wavelength at Fo


   CKT
   ! Define each block
      RWG 1 2 A^Al B^B L^L1 ER=1 RHO=1
      DEF2P 1 2 LWG1

      RWG 1 2 A^Al B^B L^D1 ER^ER RHO=1
      DEF2P 1 2 LWGD1

      RWG 1 2 A^Al B^B L^L2 ER=1 RHO=1
      DEF2P 1 2 _WG2

      RWG 1 2 A^Al B^B L^D2 ER^ER RHO=1
      DEF2P 1 2 LWGD2

      RWG 1 2 A^Ar B^B L^L3 ER=1 RHO=1
      DEF2P 1 2 RWG1

      RWG 1 2 A^Ar B^B L^D3 ER^ER RHO=1
      DEF2P 1 2 RWGD

   ! Connect the elements, and define them as LEFT and RIGHT halves.
      LWG1 1 2
      LWGD1 2 3
      LWG2 3 4
      LWGD2 4 5
      LWG2 6 5
      LWGD1 7 6
      LWG1 8 7
      DEF2P 1 8 LEFT

      RWG1 1 2
      RWGD 2 3
```

```
      RWG1 4 3
      DEF2P 1 4 RIGHT

! Connect them together with a parallel inductor and capacitor at
! both ends and define it as a two-path bandpass filter (TPBPF).
      PLC 1 0 L^Lp C^Cp
      LEFT 1 2
      RIGHT 1 2
      PLC 2 0 L^Lp C^Cp
      DEF2P 1 2 TPBPF

! Connect a capacitive window at the proper length and define
! this as the LEAD section.
      CAP 1 0 C^Cc
      RWG 1 2 A^Ag B^B L^Lc ER=1 RHO=1
      DEF2P 1 2 LEAD

! This is a filter with capacitive windows (FIL_CW).
      LEAD 1 2
      TPBPF 2 3
      LEAD 4 3
      DEF2P 1 4 FIL_CW

! Set up termination of matched load.
      RWGT 1 A^Ag B^B ER=1 RHO=1
      DEF1P 1 WEDGE


TERM
      FIL_CW WEDGE WEDGE


PROC


OUT
      FIL_CW  DB[S21]  GR1  ! Insertion loss
!     FIL_CW  DB[S11]  GR1  ! Return loss


FREQ
      SWEEP 8 13 0.05
      SWEEP 8.0 8.3 0.01
      SWEEP 10.75 11.1 0.01
      SWEEP 9.2 9.9 0.02


GRID
      RANGE 8 13 0.5
!     RANGE  9.0 10.0 0.25
!     GR1 -3 0 1
```

40

APPENDIX B. *TOUCHSTONE* DATA FILES

A. L = 100 mils
```
! FILE:  Bifurcated WG w/ dielectric 100 mils from edge
!    (BIFWG100)
! USER:  LT Gregory Miller
! DATE:  14 NOV 91
! REVISED: 19 NOV 91

# GHZ S MA R 50

! SCATTERING PARAMETERS:

! FREQ      /S11/      <S11
   8.0      0.984      149.2
   8.5      0.982      140.2
   9.0      0.976      117.4
   9.5      0.967      166.8
  10.0      0.958      142.0
  10.5      0.948      134.1
  11.0      0.937      122.1
  11.5      0.923      115.8
  12.0      0.910       97.2
```

B. L = 150 mils
```
! FILE:  Bifurcated WG w/ dielectric 150 mils from edge
!    (BIFWG150)
! USER:  LT Gregory Miller
! DATE:  14 NOV 91
! REVISED: 19 NOV 91

# GHZ S MA R 50

! SCATTERING PARAMETERS:

! FREQ      /S11/      <S11
   8.0      0.986      149.6
   8.5      0.985      142.4
   9.0      0.982      124.3
   9.5      0.975      149.8
  10.0      0.969      135.9
  10.5      0.962      126.9
  11.0      0.955      119.3
  11.5      0.947      112.8
  12.0      0.939       94.8
```

C. L = 200 mils
! FILE: Bifurcated WG w/ dielectric 200 mils from edge
!   (BIFWG200)
! USER: LT Gregory Miller
! DATE: 14 NOV 91
! REVISED: 19 NOV 91

GHZ S MA R 50

! SCATTERING PARAMETERS:

! FREQ	/S11/	<S11
8.0	0.984	150.0
8.5	0.984	142.8
9.0	0.982	130.2
9.5	0.979	148.7
10.0	0.975	131.1
10.5	0.968	126.2
11.0	0.960	117.8
11.5	0.952	110.5
12.0	0.944	96.4

D. L = 250 mils
! FILE: Bifurcated WG w/ dielectric 250 mils from edge
!   (BIFWG250)
! USER: LT Gregory Miller
! DATE: 14 NOV 91
! REVISED: 19 NOV 91

GHZ S MA R 50

! SCATTERING PARAMETERS:

! FREQ	/S11/	<S11
8.0	0.983	149.6
8.5	0.982	143.7
9.0	0.979	134.7
9.5	0.976	141.5
10.0	0.971	129.9
10.5	0.967	122.3
11.0	0.963	116.4
11.5	0.959	108.2
12.0	0.955	96.4

E. L = 300 mils
! FILE: Bifurcated WG w/ dielectric 300 mils from edge
!   (BIFWG300)
! USER: LT Gregory Miller
! DATE: 14 NOV 91
! REVISED: 19 NOV 91

```
# GHZ S MA R 50

! SCATTERING PARAMETERS:

! FREQ     /S11/      <S11
  8.0      0.985      140.1
  8.5      0.983      143.7
  9.0      0.979      136.6
  9.5      0.973      137.1
 10.0      0.968      132.9
 10.5      0.963      122.9
 11.0      0.958      115.0
 11.5      0.953      109.7
 12.0      0.948       96.4
```

APPENDIX C. DISCONTINUITY MODEL *TOUCHSTONE* CIRCUIT FILE

```
! FILE:   Two-Path Section (TPSEC)
! USER: LT Gregory Miller
! DATE: 18 OCT 91
! REVISED:  11 DEC 91
! CIRCUIT:  Two-path section with dielectric

! COMMENT:  This file examines the affect of varying the distance
!      between the edge of a long bifurcating strip in X-band
!      waveguide and a block of dielectric material in the
!      below-cutoff section.  As the dielectric block is moved
!      closer to the edge, the more its presence will change
!      S11.  This file will be used to match S11 to that found
!      experimentally using the optimizers available in
!      Touchstone.

DIM
   FREQ GHZ
   RES OH
   IND NH
   CAP PF
   LNG CM
   TIME PS
   COND /OH
   ANG DEG

VAR
   A=2.286          ! Standard WR-90 WG
   B=1.016
   Fc=6.562
   L_TOT=17         ! Total length of the structure
   L_D=1.32         ! Length of the dielectric block
   L_A1=0.762       ! Length of first air-filled section
   ER=4.61          ! Relative permittivity of block
   Lps=14.0         ! Inductor on air-filled side
   Cps=0.003        ! Capacitor on air-filled side
   Lpm # 14.0 15.21 20.0      ! Inductor on dielectric-loaded side
   Cpm # 0.0001 0.0001 0.005 ! Capacitor on dielectric-loaded side

EQN
   L_A2=L_TOT-L_A1-L_D  ! Length of remaining air-filled section
   Al=A/2               ! Width of left & right halves
   Ar=A/2

CKT
! Define LEFT and RIGHT halves
   PLC 1 0 L^Lpm C^Cpm
   RWG 1 2 A^Al B^B L^L_A1 ER=1 RHO=1
```

44

```
    RWG 2 3 A^A1 B^B L^L_D ER^ER RHO=1
    RWG 3 4 A^A1 B^B L^L_A2 ER=1 RHO=1
    DEF2P 1 4 LEFT

    PLC 1 0 L^Lps C^Cps
    RWG 1 2 A^Ar B^B L^L_TOT ER=1 RHO=1
    DEF2P 1 2 RIGHT

! Connect the halves together as a Two-Path Model (TPMOD)
    LEFT 1 2
    RIGHT 1 2
    DEF2P 1 2 TPMOD

! Set up termination of matched load
    RWGT 1 A^A B^B ER=1 RHO=1
    DEF1P 1 WEDGE

! Set up split section terminated with a matched load as a 1-port
! network and call it Loaded Two-Path Model (LD_TPMOD)
    TPMOD 1 2
    WEDGE 2
    DEF1P 1 LD_TPMOD

! Define a 1-port Two-Path WG (TPWG) based on data from the
! BIFWGXXX.S1P data file (XXX is the distance from the edge to
! the dielectric block in mils).
    S1PA 1 0 BIFWG300.S1P
    DEF1P 1 TPWG200

TERM
    LD_TPMOD WEDGE

PROC
    MOD_ERR=LD_TPMOD/TPWG300 ! The result is the angle difference

OUT
    LD_TPMOD DB[S11] GR1        ! Return loss
    LD_TPMOD MAG[S11] GR2
    LD_TPMOD ANG[S11] GR3
    LD_TPMOD S11 SC2

    TPWG300 DB[S11] GR1         ! Return loss
    TPWG300 MAG[S11] GR2
    TPWG300 ANG[S11] GR3
    TPWG300 S11 SC2

FREQ
    SWEEP 8 12 0.1
!   SWEEP 9.3 9.5 0.01

GRID
    RANGE 8 12 0.5
```

```
   GR3 90 150 10
!  RANGE 9.3 9.5 0.025

OPT
   RANGE 8 9
   MOD_ERR ANG[S11]=0
   RANGE 9.5 12
   MOD_ERR ANG[S11]=0

TOL
```

APPENDIX D. FINAL MODEL *TOUCHSTONE* CIRCUIT FILE

```
! FILE:     Two-Path Dielectric Resonator Filter (TPDRF)
! USER:     LT Gregory Miller
! DATE:     24 SEP 91
! REVISED:  16 DEC 91
! CIRCUIT:  Two-path cutoff waveguide dielecrtic resonator filter

! COMMENT:  This file is a trial of some different WG/dielectric
!       combinations.  It is based on a design in Ref.2
!
!       It simulates both halves of a split WG, with a different
!       parallel inductor and capacitor on the two paths to model
!       the losses due to the dicontinuity between the standard
!       WG and the split section.
!
!       It also incorporates capacitive windows implemented as
!       frequency-dependent capacitors.  The frequency dependence
!       is represented as an equation relating Bc/Yo to
!       capacitive window geometry found in Ref. 6.

DIM

    FREQ GHZ
    RES OH
    IND NH
    CAP PF
    LNG CM
    TIME PS
    COND /OH
    ANG RAD


VAR
    Ag=2.286 ! WR-90 WG
    Al=1.18  ! Left and right halves are not symmetric
    Ar=1.09
    B=1.016

    ER=3.78  ! Dielectric constant used by Shigesawa, et al.

    L1=0.69  ! Length of 1st & last air-filled section, main path
    L2=1.33  ! Length of 2nd & 3rd air-filled section, main path
    L3=2.01  ! Length of 1st & last air-filled section, subs path
    D1=0.40  ! Length of 1st & last er-filled section, main path
    D2=0.40  ! Length of middle er-filled section, main path
    D3=1.22  ! Length of er-filled section, subsidiary path

    Cpm=0.002 ! Value of parallel capacitor, main path (pF)
    Lpm=19.8  ! Value of parallel inductor, main path (nH)
```

```
     Cps=0.003   ! Value of parallel capacitor, subsidiary path (pF)
     Lps=14.0    ! Value of parallel inductor, subsidiary path (nH)

     d=0.1138    ! Size of capacitive window (cm)

EQN
! Equations for FREQ-dependent element (capacitive window)
     PI=3.1415927
     Fc=6.562                        ! Cutoff frequency
     Fo=9.5                          ! Center frequency
     lam=30/FREQ                     ! Wavelength in cm if FREQ in GHz
     Gfac=(1-(Fc/FREQ)**2)**0.5      ! Guide factor
     lamg=lam/Gfac                   ! Guided wavelength
     Zo=(120*PI*2*B/Ag)/Gfac         ! Characteristic impedance
     Bc_Yo=(4*B/lamg)*LN(1/SIN(PI*d/(2*b)))! Normalized susceptance
     Cc=1000*Bc_Yo/(Zo*2*PI*FREQ)    ! FREQ-dependent capacitance
     Gfaco=(1-(Fc/Fo)**2)**0.5       ! Guide factor at Fo
     Lc=0.5*(30/Fo)/Gfaco            ! Half a guided wavelength at Fo


CKT
! Define each block
     RWG  1 2  A^Al  B^B  L^L1  ER=1  RHO=1
     DEF2P  1 2  LWG1

     RWG  1 2  A^Al  B^B  L^D1  ER^ER  RHO=1
     DEF2P  1 2  LWGD1

     RWG  1 2  A^Al  B^B  L^L2  ER=1  RHO=1
     DEF2P  1 2  LWG2

     RWG  1 2  A^Al  B^B  L^D2  ER^ER  RHO=1
     DEF2P  1 2  LWGD2

     RWG  1 2  A^Ar  B^B  L^L3  ER=1  RHO=1
     DEF2P  1 2  RWG1

     RWG  1 2  A^Ar  B^B  L^D3  ER^ER  RHO=1
     DEF2P  1 2  RWGD

! Connect the elements, and define them as LEFT and RIGHT halves.
     PLC  1 0  L^Lpm  C^Cpm
     LWG1  1 2
     LWGD1  2 3
     LWG2  3 4
     LWGD2  4 5
     LWG2  6 5
     LWGD1  7 6
     LWG1  8 7
     PLC  8 0  L^Lpm  C^Cpm
     DEF2P  1 8  LEFT
```

```
      PLC  1  0  L^Lps  C^Cps
      RWG1  1  2
      RWGD  2  3
      RWG1  4  3
      PLC  4  0  L^Lps  C^Cps
      DEF2P  1  4  RIGHT

! Connect them together and define it as a two-path bandpass
! filter (TPBPF).
      LEFT  1  2
      RIGHT  1  2
      DEF2P  1  2  TPBPF

! Connect a capacitive window at the proper length and define
! this as the LEAD section.
      CAP  1  0  C^Cc
      RWG  1  2  A^Ag  B^B  L^Lc  ER=1  RHO=1
      DEF2P  1  2  LEAD

! This is a filter with capacitive windows (FIL_CW).
      LEAD  1  2
      TPBPF  2  3
      LEAD  4  3
      DEF2P  1  4  FIL_CW

! Set up termination of matched load.
      RWGT  1  A^Ag  B^B  ER=1  RHO=1
      DEF1P  1  WEDGE


TERM
    FIL_CW  WEDGE  WEDGE

PROC


OUT
    FIL_CW   DB[S21]   GR1   ! Insertion loss
!    FIL_CW   DB[S11]   GR1   ! Return loss


FREQ
    SWEEP  8  13  0.05
    SWEEP  8.0  8.3  0.01
    SWEEP  10.75  11.1  0.01
    SWEEP  9.2  9.9  0.02


GRID
    RANGE  8  13  0.5
!    RANGE  9.0  10.0  0.25
!    GR1  -3  0  1
```

APPENDIX E. SEPARATED PATHS *TOUCHSTONE* CIRCUIT FILE

```
! FILE:      Left and Right Paths (L_R_PATH)
! USER:      LT Gregory Miller
! DATE:      12 DEC 91
! REVISED:   13 DEC 91
! CIRCUIT:   Two-path cutoff waveguide dielecrtic resonator filter

! COMMENT:  This file is a trial of some different WG/dielectric
!       combinations.  It is based on a design in Ref.2
!
!       It simulates both halves of a split WG, with a different
!       parallel inductor and capacitor on the two paths to model
!       the losses due to the dicontinuity between the standard
!       WG and the split section.
!
!       It also incorporates capacitive windows implemented as
!       frequency-dependent capacitors.  The frequency dependence
!       is represented as an equation  relating Bc/Yo to
!       capacitive window geometry found in Ref. 6.
!
!       This file looks specifically at the magnitude and phase
!       of S21 of the main and subsidiary paths.

DIM

   FREQ GHZ
   RES OH
   IND NH
   CAP PF
   LNG CM
   TIME PS
   COND /OH
   ANG DEG

VAR
   Ag=2.286  ! WR-90 WG spilt in half
   Al=1.18   ! left and right halves are not symmetric
   Ar=1.09
   B=1.016

   ER=3.78   ! Dielectric constant used by Shigesawa, et al.

   L1=0.69   ! Length of 1st & last air-filled section, main path
   L2=1.33   ! Length of 2nd & 3rd air-filled section, main path
   L3=2.01   ! Length of 1st & last air-filled section, subs path
   D1=0.40   ! Length of 1st & last er-filled section, main path
   D2=0.40   ! Length of middle er-filled section, main path
   D3=1.22   ! Length of er-filled section, subsidiary path
```

```
       Cpm=0.002 ! Value of parallel capacitor, main path (pF)
       Lpm=19.8  ! Value of parallel inductor, main path (nH)
       Cps=0.003 ! Value of parallel capacitor, subsidiary path (pF)
       Lps=14.0  ! Value of parallel inductor, subsidiary path (nH)
       d=0.1138  ! Size of capacitive window (cm)

   EQN
   ! Equations for FREQ-dependent element (capacitive window)
       PI=3.1415927
       Fc=6.562                      ! Cutoff frequency
       Fo=9.5                        ! Center frequency
       lam=30/FREQ                   ! Wavelength in cm if FREQ in GHz
       Gfac=(1-(Fc/FREQ)**2)**0.5    ! Guide factor
       lamg=lam/Gfac                 ! Guided wavelength
       Zo=(120*PI*2*B/Ag)/Gfac       ! Characteristic impedance
       Bc_Yo=(4*B/lamg)*LN(1/SIN(180*d/(2*b)))!Normalized susceptance
       Cc=1000*Bc_Yo/(Zo*2*PI*FREQ)  ! FREQ-dependent capacitance
       Gfaco=(1-(Fc/Fo)**2)**0.5     ! Guide factor at Fo
       Lc=0.5*(30/Fo)/Gfaco          ! Half a guided wavelength at Fo


   CKT
   ! Define each block
       RWG 1 2 A^Al B^B L^L1 ER=1 RHO=1
       DEF2P 1 2 LWG1

       RWG 1 2 A^Al B^B L^D1 ER^ER RHO=1
       DEF2P 1 2 LWGD1

       RWG 1 2 A^Al B^B L^L2 ER=1 RHO=1
       DEF2P 1 2 LWG2

       RWG 1 2 A^Al B^B L^D2 ER^ER RHO=1
       DEF2P 1 2 LWGD2

       RWG 1 2 A^Ar B^B L^L3 ER=1 RHO=1
       DEF2P 1 2 RWG1

       RWG 1 2 A^Ar B^B L^D3 ER^ER RHO=1
       DEF2P 1 2 RWGD

   ! Connect the elements and define them as LEFT and RIGHT halves.
       PLC 1 0 L^Lpm C^Cpm
       LWG1 1 2
       LWGD1 2 3
       LWG2 3 4
       LWGD2 4 5
       LWG2 6 5
       LWGD1 7 6
       LWG1 8 7
       PLC 8 0 L^Lpm C^Cpm
       DEF2P 1 8 LEFT
```

```
    PLC 1 0 L^Lps C^Cps
    RWG1 1 2
    RWGD 2 3
    RWG1 4 3
    PLC 4 0 L^Lps C^Cps
    DEF2P 1 4 RIGHT


! DUMMY sides with no dielectric blocks in them will be needed
    PLC 1 0 L^Lpm C^Cpm
    RWG 1 2 A^Al B^B L=5.24 ER=1 RHO=1
    PLC 2 0 L^Lpm C^Cpm
    DEF2P 1 2 DUM_L

    PLC 1 0 L^Lpm C^Cps
    RWG 1 2 A^Ar B^B L=5.24 ER=1 RHO=1
    PLC 2 0 L^Lpm C^Cps
    DEF2P 1 2 DUM_R

! Connect a capacitive window at the proper length and define
! this as the LEAD section.
    CAP 1 0 C^Cc
    RWG 1 2 A^Ag B^B L^Lc ER=1 RHO=1
    DEF2P 1 2 LEAD

! Set up left and right halves by themselves.
! Connect the left and right sides to the lead and define them as
! MAIN path and SUBSidiary path, respectively.
    LEAD 1 2
    LEFT 2 3
    DUM_R 2 3
    LEAD 4 3
    DEF2P 1 4 MAIN

    LEAD 1 2
    RIGHT 2 3
    DUM_L 2 3
    LEAD 4 3
    DEF2P 1 4 SUBS

! Check the lead section by itself.
    LEAD 1 2
    PLC 2 0 L^Lpm C^Cpm
    PLC 2 0 L^Lps C^Cps
    DEF2P 1 2 LEAD_D

! Set up termination of matched load.
    RWGT 1 A^Ag B^B ER=1 RHO=1
    DEF1P 1 WEDGE


TERM
    MAIN WEDGE WEDGE
```

```
      SUBS WEDGE WEDGE
      LEAD_D WEDGE WEDGE

PROC


OUT
      MAIN    DB[S21]    GR1A
      MAIN    ANG[S21]    GR1
      SUBS    DB[S21]    GR2A
      SUBS    ANG[S21]    GR2
      LEAD_D  DB[S21]    GR3A
      LEAD_D  ANG[S21]    GR3


FREQ
      SWEEP 8 13 0.05
      SWEEP 8.0 8.2 0.01
      SWEEP 9.3 9.8 0.01
      SWEEP 10.75 10.95 0.01
      SWEEP 12.8 13 0.01

GRID
      RANGE 8 13 0.5
      GR1 -180 180 20
      GR1A -95 0
      GR2 -180 180 20
      GR2A -95 0
      GR3 -180 180 20
      GR3A -6 0

OPT

TOL
```

APPENDIX F. OPTIMIZED FILTER DESIGN *TOUCHSTONE* CIRCUIT FILE

```
! FILE:     A Two-Path Cutoff Waveguide Dielectric Resonator
!           Filter Designed w/ optimizer (DES_O)
! USER:     LT Gregory Miller
! DATE:     20 DEC 91
! REVISED:  9 JAN 92
! CIRCUIT:  Two-path cutoff waveguide dielecrtic resonator filter

! COMMENT:  This file is the first attempt to design a two-path
!           cutoff waveguide dielectric resonator filter.  It
!           simulates both halves of a split WG, with a parallel
!           inductor and capacitor to model the losses due to the
!           dicontinuity between the standard WG and the split
!           section.
!
!           It also incorporates capacitive windows similar to
!           previous programs.  They are implemented as
!           frequency-dependent capacitors.  The frequency dependence
!           is represented as an equation relating Bc/Yo to
!           capacitive window geometry found in Ref. 6.
!
!           Optimizers are used to find values of D1, D2, D3, L2, L3,
!           and d.  The main path will first be specified according
!           to the passband requirements, and then the subsidiary
!           path according to stopband requirements.  To do this, the
!           subsidiary path is first replaced by a long below cutoff
!           section (7 cm should be long enough).  Only after the
!           values for the main path are set will the subsidiary path
!           be found.  L1 must be specified before optimization can
!           begin because it is associated with the discontinuity
!           elements.

DIM

    FREQ GHZ
    RES OH
    IND NH
    CAP PF
    LNG CM
    TIME PS
    COND /OH
    ANG RAD

VAR
    Ag=2.286 ! WR-90 WG
    Al=1.143 ! Left and right halves are symmetric
    Ar=1.143
    B=1.016
```

```
        ER=2.54   ! Dielectric constant

        L1=0.762 ! Length of 1st & last air-filled section, main path
        L2\1.50883 ! Length of 2nd & 3rd air-filled section, main path
        D1\0.63037 ! Length of 1st & last er-filled section, main path
        D2#0.5 0.60423 0.66 ! Length of middle er-filled section, main
                  ! path
        D3=1.74   ! Length of er-filled section, susidiary path

        Cpm=0.001 ! Value of parallel capacitor, main path (pF)
        Lpm=15.21 ! Value of parallel inductor, main path (nH)
        Cps=0.003 ! Value of parallel capacitor, subsidiary path (pF)
        Lps=14.0  ! Value of parallel inductor, subsidiary path (nH)

        d\0.14934 ! Size of capacitive window (cm)

    EQN
        L_TOT=2*(L1+L2+D1)+D2   ! Total length of filter
        L3=(L_TOT-D3)/2         ! Length of 1st & last air-filled
                               ! section, subs path

    ! Equations for FREQ-dependent element (capacitive window)
        PI=3.1415927
        Fc=6.562                    ! Cutoff frequency (GHz)
        Fo=10.5                     ! Center frequency (GHz)
        lam=30/FREQ                 ! Wavelength in cm if FREQ in GHz
        Gfac=(1-(Fc/FREQ)**2)**0.5  ! Guide factor
        lamg=lam/Gfac               ! Guided wavelength
        Zo=(120*PI*2*B/Ag)/Gfac     ! Characteristic impedance
        Bc_Yo=(4*B/lamg)*LN(1/SIN(PI*d/(2*b)))! Normalized susceptance
        Cc=1000*Bc_Yo/(Zo*2*PI*FREQ) ! FREQ-dependent capacitance
        Gfaco=(1-(Fc/Fo)**2)**0.5   ! Guide factor at Fo
        Lc=0.5*(30/Fo)/Gfaco        ! Half a guided wavelength at Fo

    CKT
    ! Define each block
        RWG 1 2 A^Al B^B L^L1 ER=1 RHO=1
        DEF2P 1 2 LWG1

        RWG 1 2 A^Al B^B L^D1 ER^ER RHO=1
        DEF2P 1 2 LWGD1

        RWG 1 2 A^Al B^B L^L2 ER=1 RHO=1
        DEF2P 1 2 LWG2

        RWG 1 2 A^Al B^B L^D2 ER^ER RHO=1
        DEF2P 1 2 LWGD2

        RWG 1 2 A^Ar B^B L^L3 ER=1 RHO=1
        DEF2P 1 2 RWG1
```

```
      RWG 1 2 A^Ar B^B L^D3 ER^ER RHO=1
      DEF2P 1 2 RWGD

! Connect the elements, and define them as LEFT and RIGHT halves.
! First the LEFT half (main path).
      PLC 1 0 L^Lpm C^Cpm
      LWG1 1 2
      LWGD1 2 3
      LWG2 3 4
      LWGD2 4 5
      LWG2 6 5
      LWGD1 7 6
      LWG1 8 7
      PLC 8 0 L^Lpm C^Cpm
      DEF2P 1 8 LEFT

! The RIGHT half (subsidiary path) is replaced by a long below
! cutoff section during the design of the main path.  After the
! main path is determined, the subsidiary path is designed.
      PLC 1 0 L^Lps C^Cps
      RWG1 1 2
      RWGD 2 3
      RWG1 4 3
!     RWG 1 2 A^Ar B^B L=7 ER=1 RHO=1
      PLC 2 0 L^Lps C^Cps
      DEF2P 1 2 RIGHT

! Connect them together and define it as a two-path bandpass
! filter (TPBPF).
      LEFT 1 2
      RIGHT 1 2
      DEF2P 1 2 TPBPF

! Connect a capacitive window at the proper length and define it
! as the LEAD section
      CAP 1 0 C^Cc
      RWG 1 2 A^Ag B^B L^Lc ER=1 RHO=1
      DEF2P 1 2 LEAD

! This is a filter with capacitive windows (FIL_CW).
      LEAD 1 2
      TPBPF 2 3
      LEAD 4 3
      DEF2P 1 4 FIL_CW

! Set up termination of matched load
      RWGT 1 A^Ag B^B ER=1 RHO=1
      DEF1P 1 WEDGE


TERM
      FIL_CW WEDGE WEDGE
```

```
PROC

OUT
   FIL_CW   DB[S21]   GR1   ! Insertion loss
!   FIL_CW   DB[S11]   GR1   ! Return loss

FREQ
   SWEEP 8 13 0.05
   SWEEP 10.3 10.7 0.02
   SWEEP 9.1 9.8 0.02
   SWEEP 10.8 11.1 0.02
   SWEEP 11.8 12.2 0.02

GRID
   RANGE 8 13 0.5
!   RANGE   10 11 0.25
!   GR1 -1 0 0.1

OPT
   RANGE 10.35 10.65
   FIL_CW DB[S21] > -0.1

TOL
```

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